

## **VERSATILE METROLOGY SOLUTION USING A** LARGE HOLOGRAPHIC STITCHING TECHNIQUE

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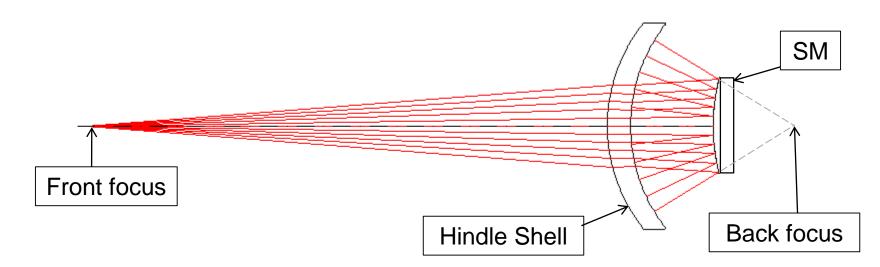
## Outline



- Convex Optical Metrology Primer
- Convex Versatile Metrology Technique Primer
- Holographic Testing Breadboard Demo
- LSST Test Configuration

#### Convex Optical Metrology Primer: Hindle Shell Test





#### Materials Needed

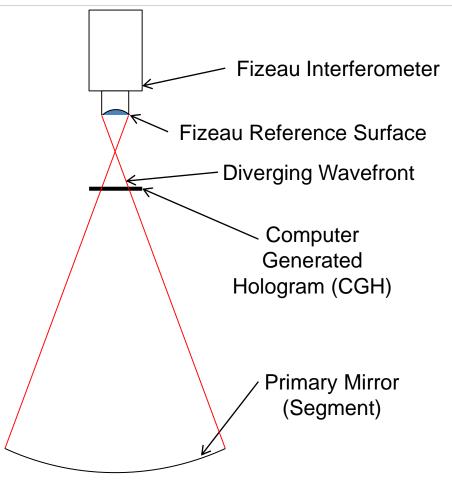
- Hindle Shell
- Calibration Sphere

#### • Example of optical design for Hindle test of ~20" asphere

- Hindle diameter ~35"
- 3.5" of sag on concave surface
- Transmissive quality critical
- Presents significant schedule and budget challenges for convex optics



- Standard Accepted Test Configuration for Primary Mirror (Segment)
- A CGH is used to convert a spherical wavefront coming from the interferometer into an aspheric wavefront to match the intended prescription of the Primary Mirror
- Three degree of freedom alignment of the interferometer to the CGH is critical
- Five degree of freedom alignment of the Primary Mirror to the CGH is critical
  - 6 DOF for off-axis segment
- This configuration does not work for convex mirrors
  - The rays would need to start from a test aperture that is larger than the optic to be tested, to converge toward the center of curvature

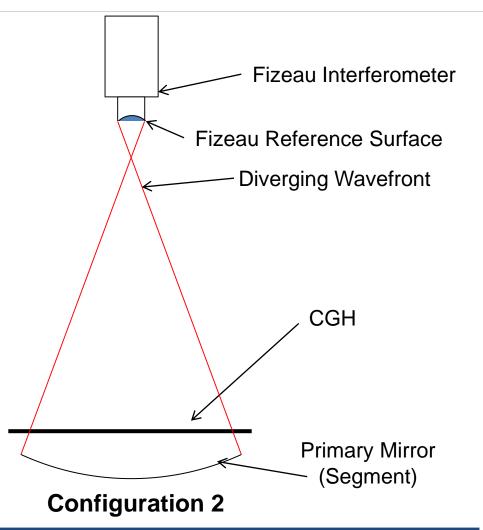


#### **Configuration 1**

This test method has been used for many programs including the JWST Primary Mirror Segments



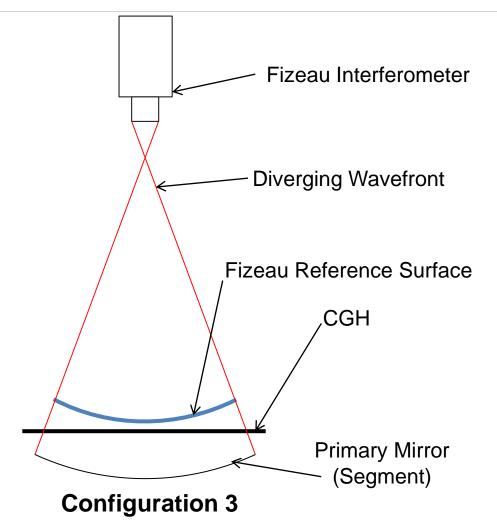
- The PM test could easily be reconfigured to look like this
  - The Phase Equation defining the CGH is more easily defined
    - This configuration is just the aspheric departure of the mirror under test
    - The typical configuration is typically extremely hyperbolic with many higher order terms (can be > 10 terms to define properly)
- This isn't typically done because the small CGH is much easier to obtain
- The configuration as drawn still requires careful alignment between the interferometer and the CGH; and the CGH to the PM
  - Z distance between the CGH and PM is considerably easier to monitor



Repositioning of the CGH simplifies the test



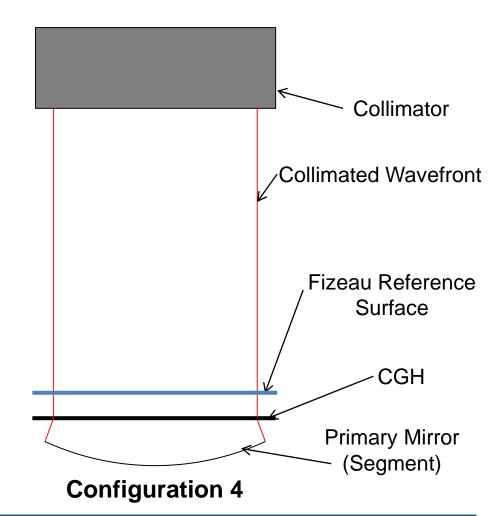
- All of the same alignment requirements apply
  - 3 DOF reference to CGH
  - 5 DOF CGH to Mirror
  - The close proximity of these surfaces to one another simplifies the monitoring of this alignment



Moving the Fizeau Reference Surface does little to change the nature of the test



- The alignment of the Fizeau reference surface to the CGH and the CGH to the mirror are still important
  - The collimated input simplifies the alignment of the Fizeau Reference to the CGH
  - 2 DOF (tilt/tilt) alignment only
- The CGH prescription now includes the power difference between the flat and the nominal RoC
  - Still a more simple phase equation than the Configuration 1
- Compressing the cavity can reduce noise



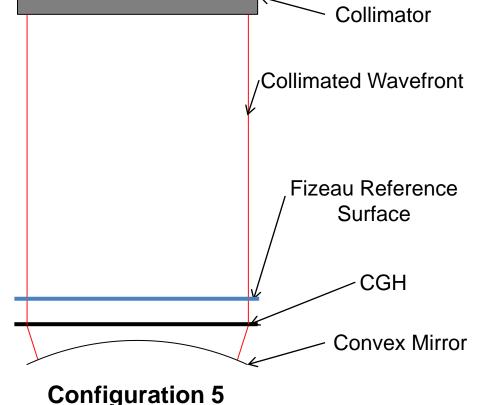
Changing the input wavefront to a collimated beam is a conceptually trivial modification

#### Versatile Metrology Solution Using a Large Holographic Stitching Technique

#### Convex Versatile Metrology Technique Primer

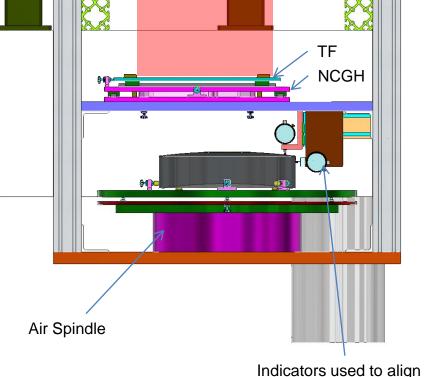
- In practice there is no difference between this test configuration and the one described in the previous slide.
- The application of this test technology to the LSST M2 will require all of the same attention to error sources as is paid to the test of a primary mirror as described in Configuration 1
- For very large optics, such as LSST M2, this test needs to be done as a sub-aperture test
  - Any single subaperture measurement of M2 is nearly identical to a primary mirror segment measurement ٠
  - Using a large number of subapertures ultimately reduces the uncertainty of • the test wavefront

Adapting this test to a convex mirror is just a change in the sign of the diffraction order





- Collimated light passes through transmissive CGH (transmissive null)
- Light reflects off surface under test, back through CGH and collimator to camera
- · Part rotates on precision air spindle
- Tilt carrier allows for instantaneous phase collection of high density sub-aperture interferograms
- Air spindle encoder triggers camera data acquisition for multiple overlapping subapertures
- Post processing software stitches subaperture data
  - Demodulates interferogram to obtain phase map using tilt carrier method
  - Stitches sub-apertures using angular encoder knowledge



12" collimated beam

incident on TF

test optic to Spindle axis

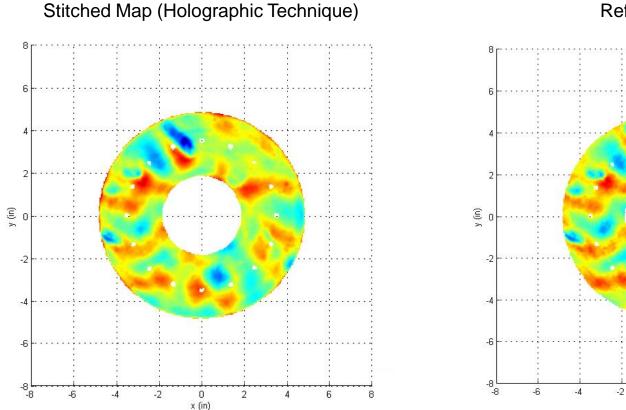






Used Holographic Test method to measure previously characterized convex surface





**Reference Map** 

Agreement within 0.008 $\lambda$  RMS SFE, consistent with typical PM test uncertainty.

0

x (in)

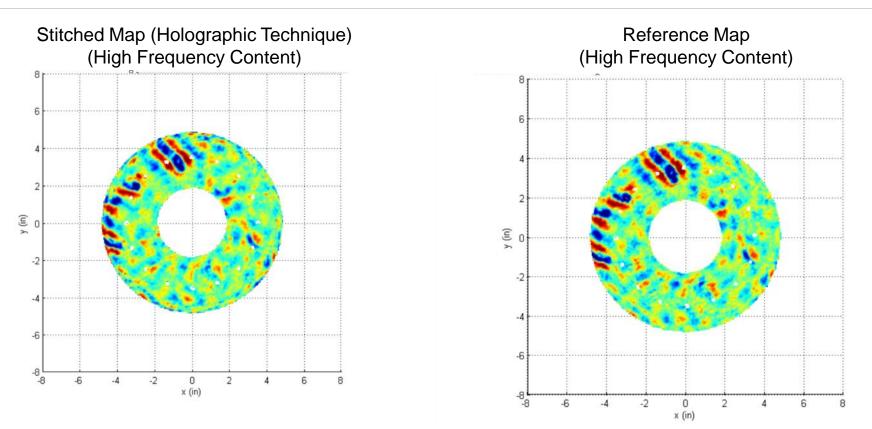
2

4

6

8



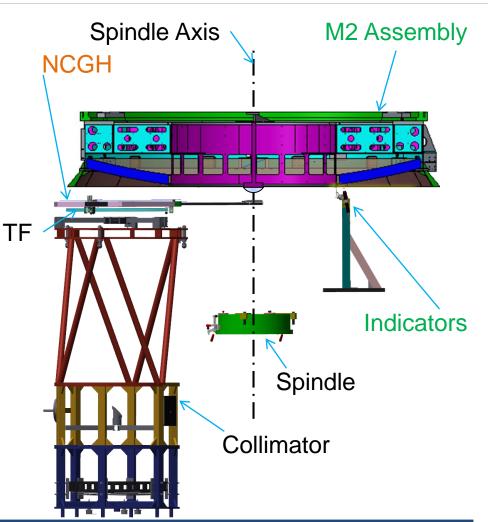


Agreement of high frequency surface content demonstrates stitching artifacts do not impact surface measurement accuracy

# **LSST Test Configuration**



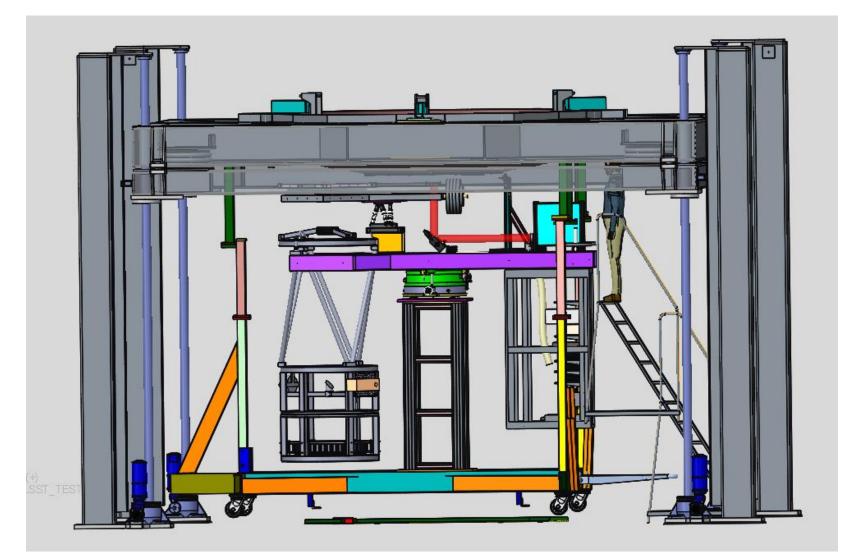
- Fizeau test configuration
  - · Collimated wavefront in
  - Flat test plate (Transmission Flat)
  - CGH (in test path only) used to diffract wavefront to null condition for M2
- Test Plate together with Nulling CGH and Alignment Reference makes up the Monolithic Holographic Assembly Testplate (MHAT)
- The MHAT test aperture covers the full radius of the M2 annulus
- M2 remains stationary. Test set components (interferometer, collimator, MHAT) rotate on spindle



The M2 test is a sub-aperture version of the test described as Configuration 5

#### **Test Design Overview**

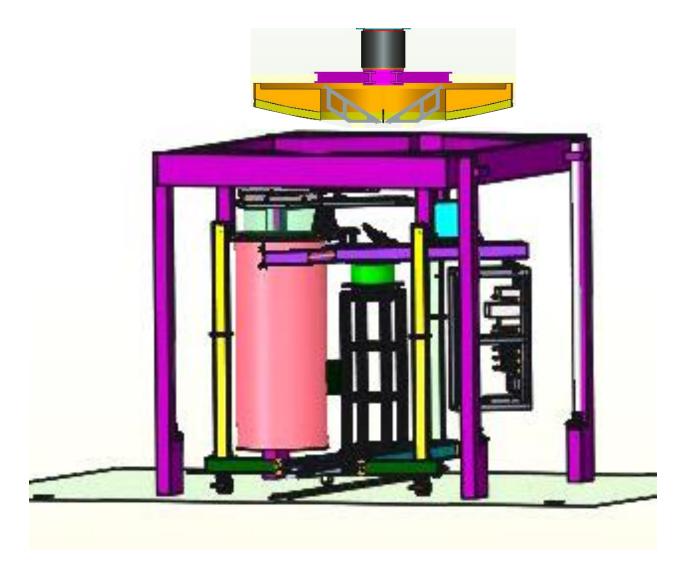




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#### **LSST** Test Tower Rotation





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