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# Modeling of Cryogenic Heated-Tube Flow Boiling Experiments of Hydrogen and Helium with GFSSP

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# Introduction

- Accurate prediction of two-phase flow boiling is required to design and analyze cryogenic transfer systems.
- Poor models penalize us: increased margins and higher costs.
- Two types of flow boiling in cryogenic transfer
  - Quenching / Chill Down (Unsteady)
  - Heating (Steady)
- Many boiling correlations are based on experimental data with water and refrigerants, rather than cryogenic fluids.
- Purdue University has assembled a cryogenic database of thousands of data points from heated tube experiments since 1959.
  - LHe, LH<sub>2</sub>, LNe, LN<sub>2</sub>, LAr, LCH<sub>4</sub>



# Purdue Universal Cryogenic Flow Boiling Correlation

- Onset of Nucleate Boiling (ONB)
- Nucleate Boiling (NB)
  - Nominal inlet conditions
  - High-quality inlet conditions
- Critical Heat Flux (CHF) as a function of axial distance  $Z$ 
  - Departure from Nucleate Boiling (DNB)
  - Dryout (DRY)
- Film Boiling (FB)
  - Dispersed Flow Film Boiling (DFFB)
    - Saturated
    - Superheated
  - Inverted Annular Film Boiling (IAFB)



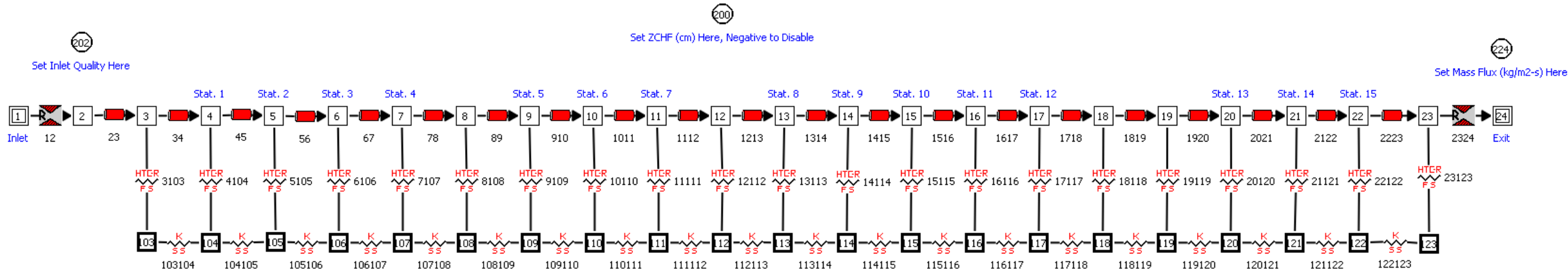
# GFSSP Overview

- GFSSP stands for Generalized Fluid System Simulation Program.
- It is a general-purpose computer program to compute pressures, temperatures, and flow rates in a fluid network.
- Fluid networks are discretized into nodes and branches.
  - Mass and energy equations are solved in the fluid nodes to get pressures and enthalpies/temperatures.
  - Momentum equation is solved in the branches to get flow rates.
  - Solid energy equation is solved in the solid nodes to get wall temperatures.
- Convection and pressure drop correlations can be programmed in Fortran user subroutines.



# Lewis LH2 (1962)

Lewis 1962, LH2 Upward Flow

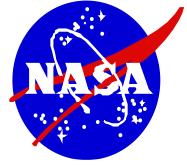


$L = 16.125 \text{ in} = 40.96 \text{ cm}$

$D_i = 0.555 \text{ in} = 1.4097 \text{ cm}$

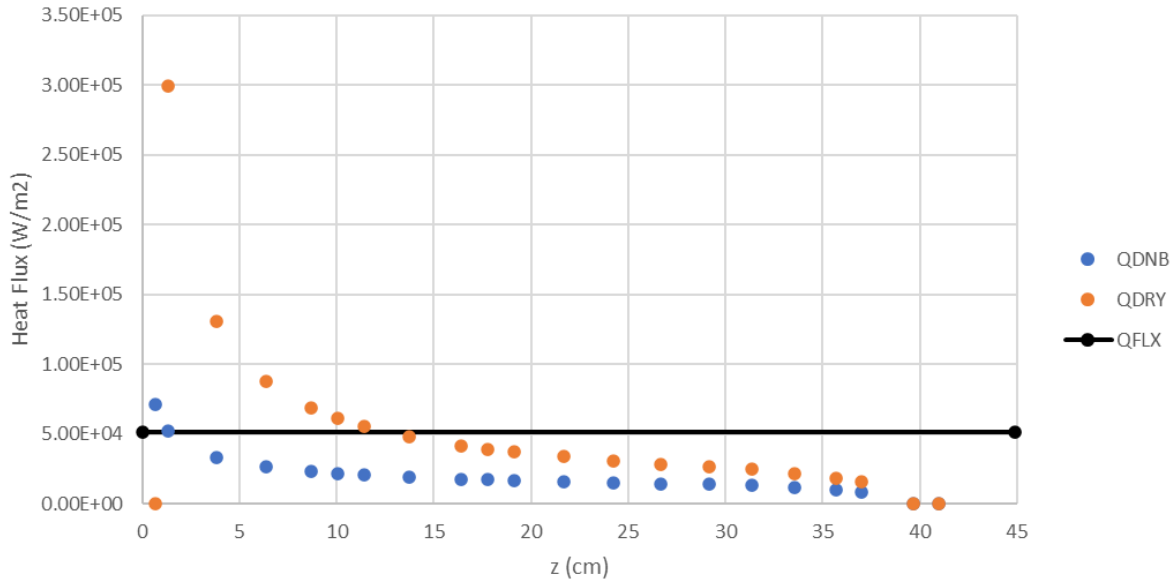
- 28 runs
- $L = 41 \text{ cm}$
- $ID = 1.41 \text{ cm}$
- $t = 0.089 \text{ cm}$
- Stainless Steel

- $P: 207\text{-}355 \text{ kPa}$
- $G: 4\text{-}12 \text{ kg/m}^2\text{-s}$
- $Q: 29\text{-}57 \text{ kW/m}^2$
- Pipe lengths are set so that nodes match TC locations.



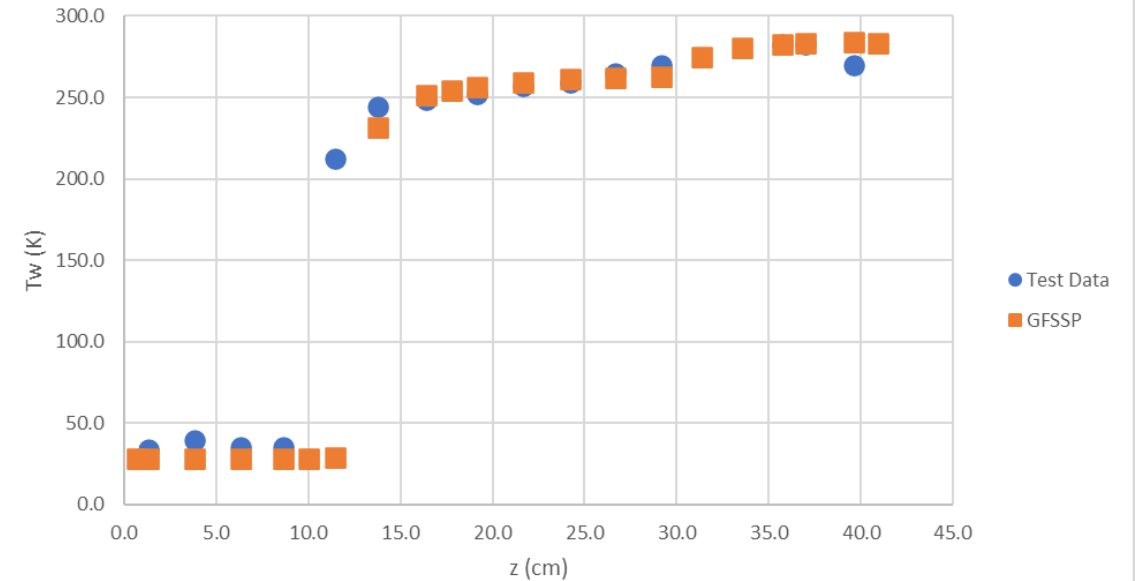
# Lewis LH2 (1962), Run 306

Lewis 1962, LH2, Run 306  
Heat Flux (W/m<sup>2</sup>)

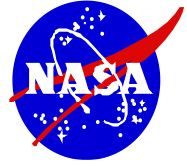


- Critical length ( $Z_{CHF}$ ) is determined where the CHF curve intersects the test heat flux.
- Reported  $Z_{CHF} = 10.2$  cm
- Predicted  $Z_{CHF} = 12.3$  cm

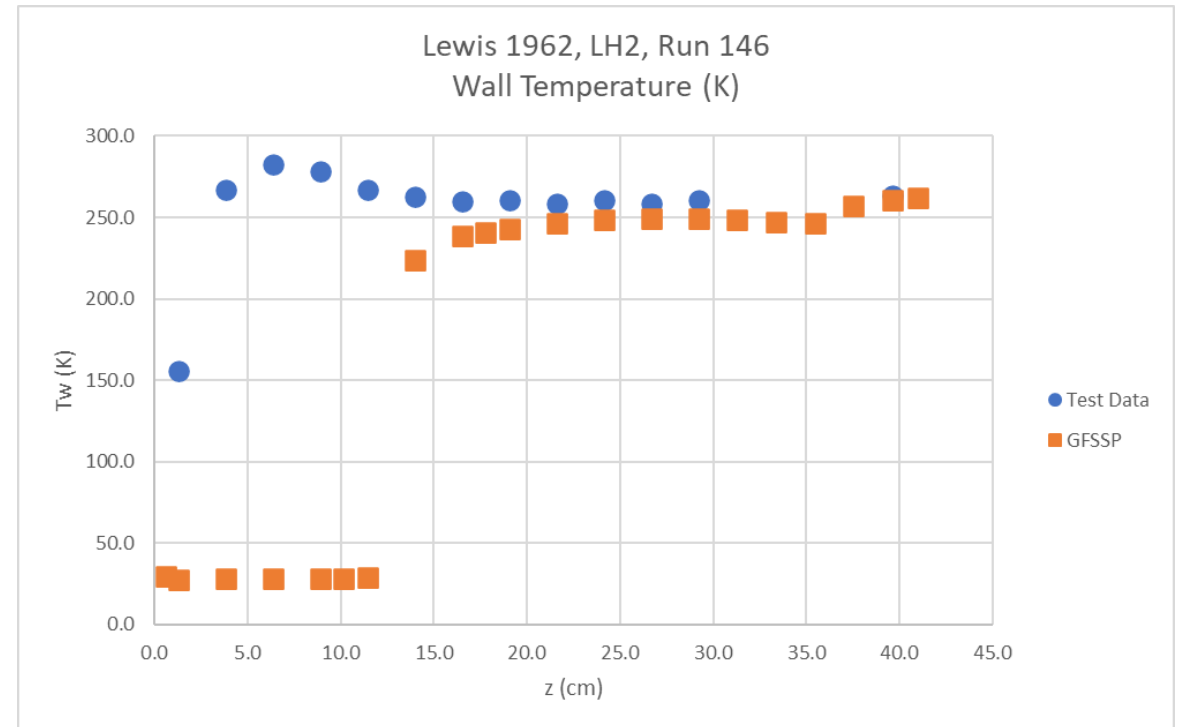
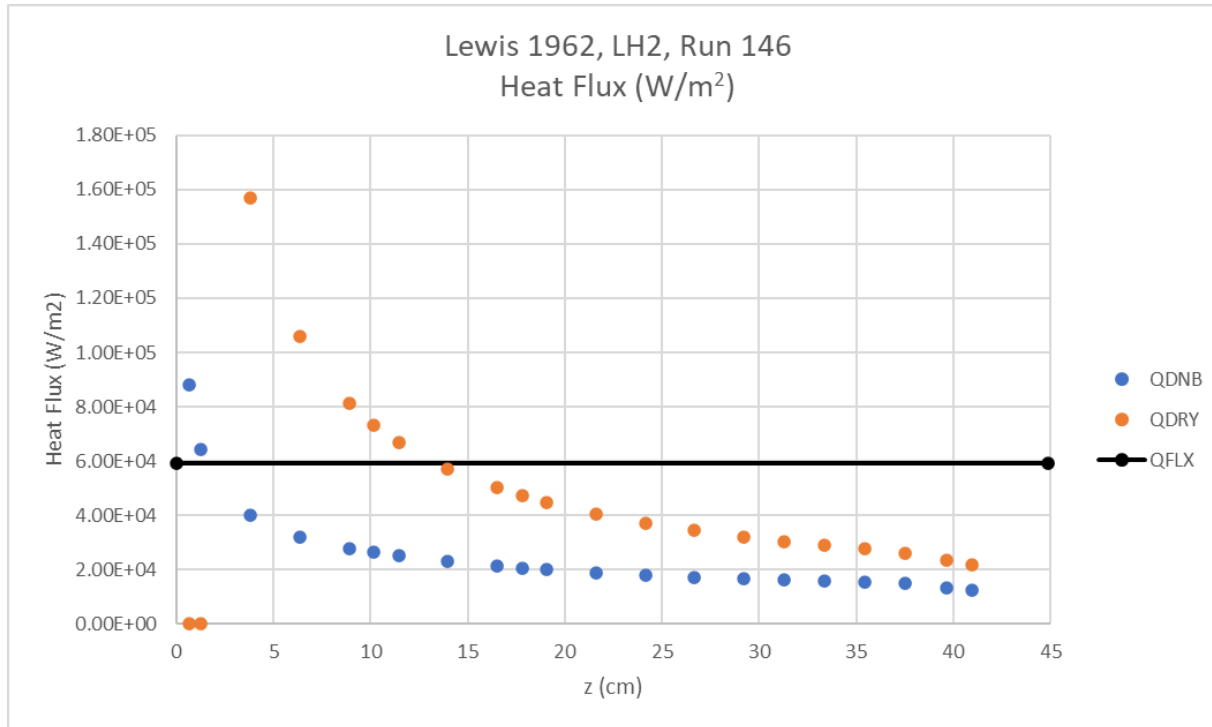
Lewis 1962, LH2, Run 306  
Wall Temperature (K)



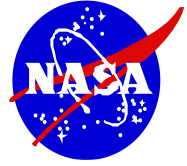
- Because of error in  $Z_{CHF}$ , wall temperature is under-predicted at 11.4 cm.



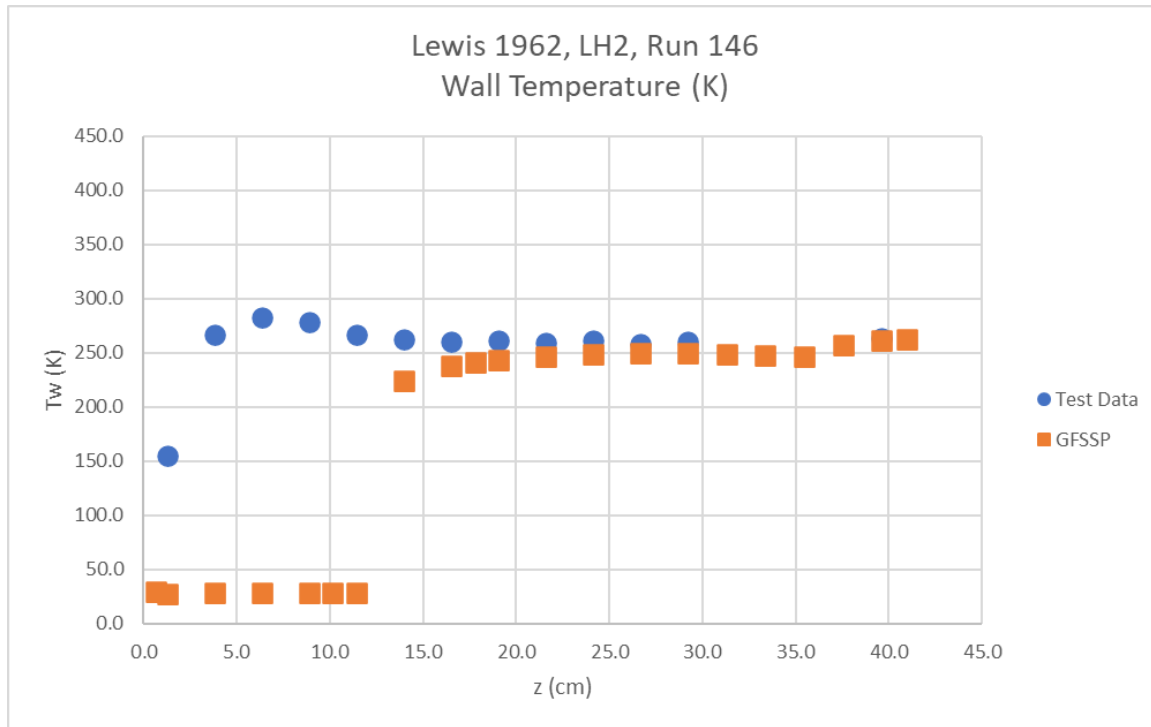
# Lewis LH2 (1962), Run 146



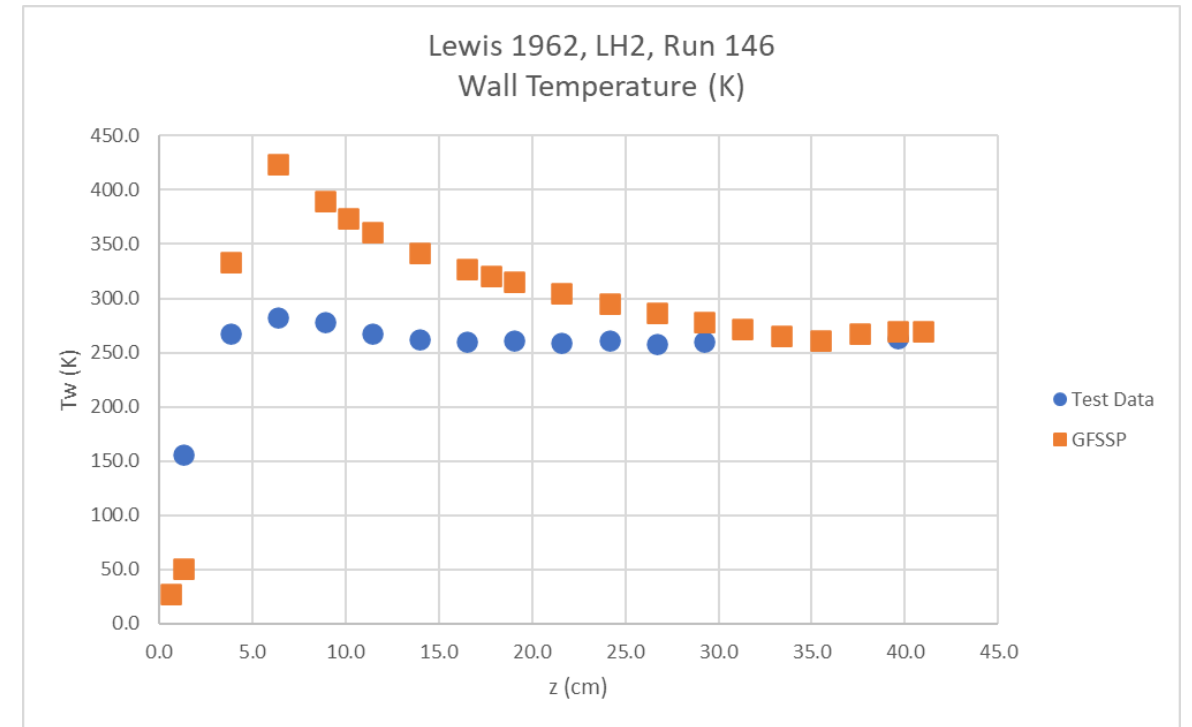
- Code chose DRY instead of DNB.
- Reported  $Z_{\text{CHF}} \approx 0$  cm
- Predicted  $Z_{\text{CHF}} = 13.1$  cm



# Lewis LH2 (1962), Run 146



Finding ZCHF, MAPE = 38%



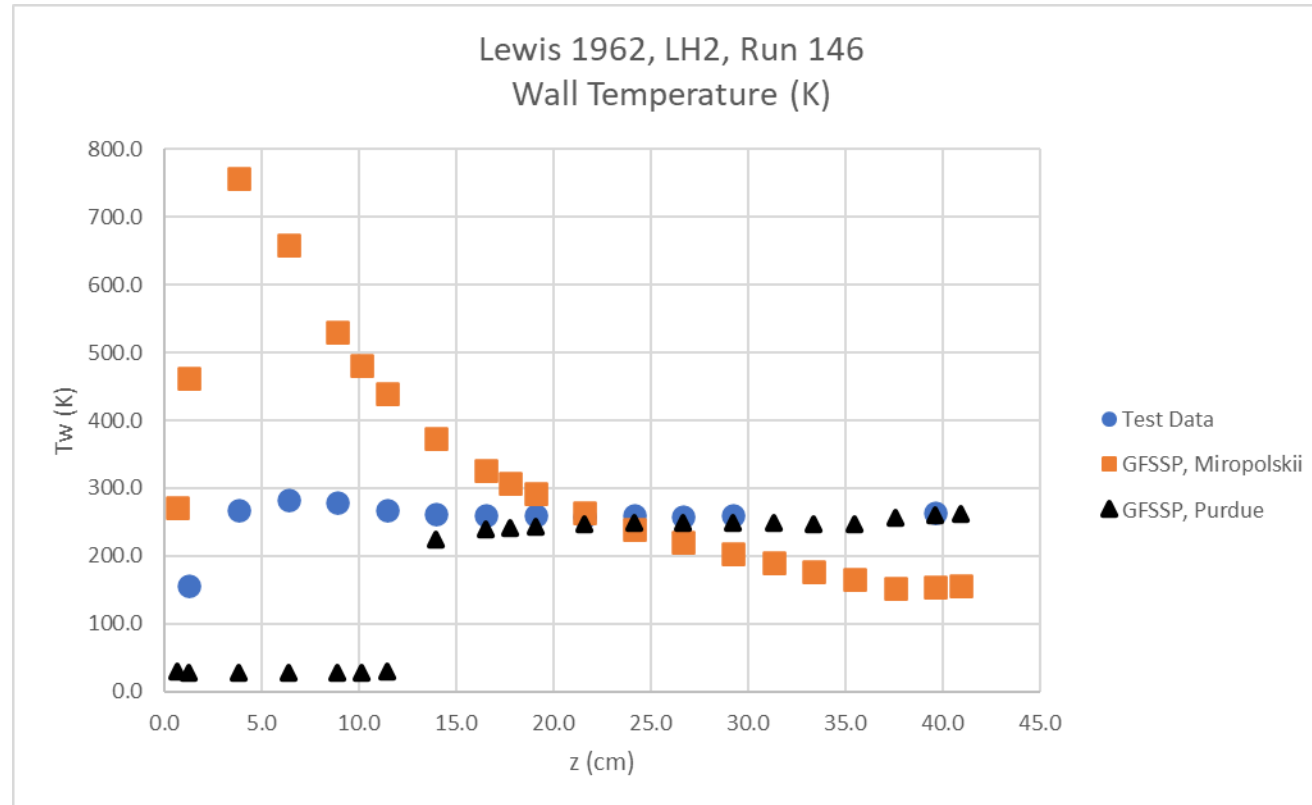
Fixing ZCHF, MAPE = 27%

- To better evaluate performance of NB and FB correlations, all runs were performed twice: Finding  $Z_{CHF}$  and Fixing  $Z_{CHF}$ .





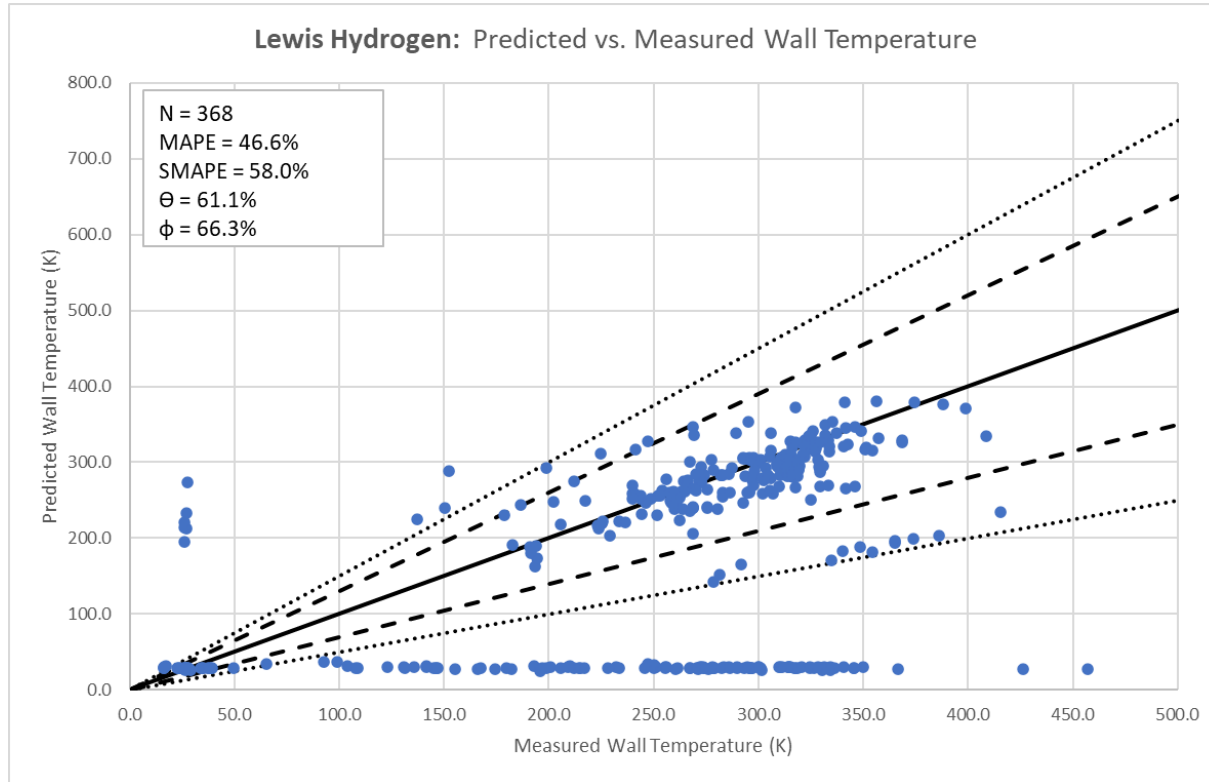
# Lewis LH2 (1962), Run 146



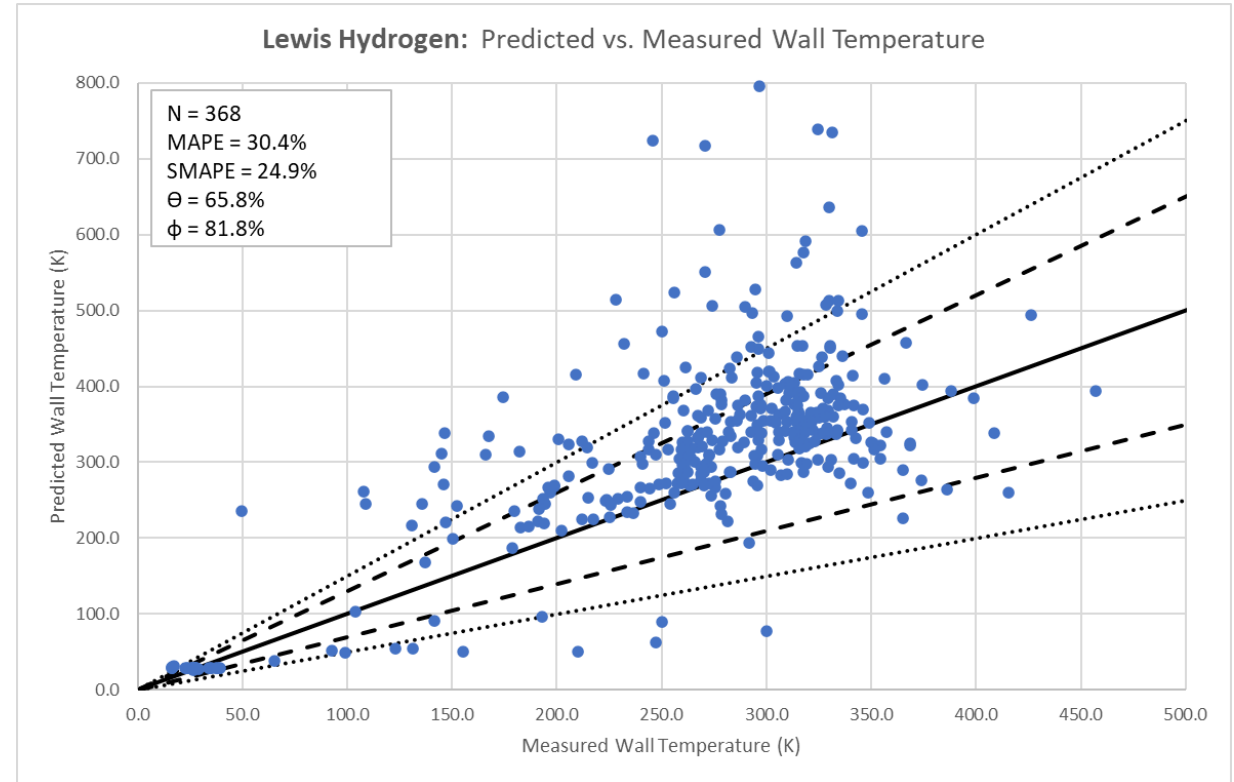
- The Purdue correlations show an improvement over the Miropolskii film boiling correlation built into GFSSP (MAPE: 38% vs. 64%).



# Lewis LH2 (1962), Parity Plots



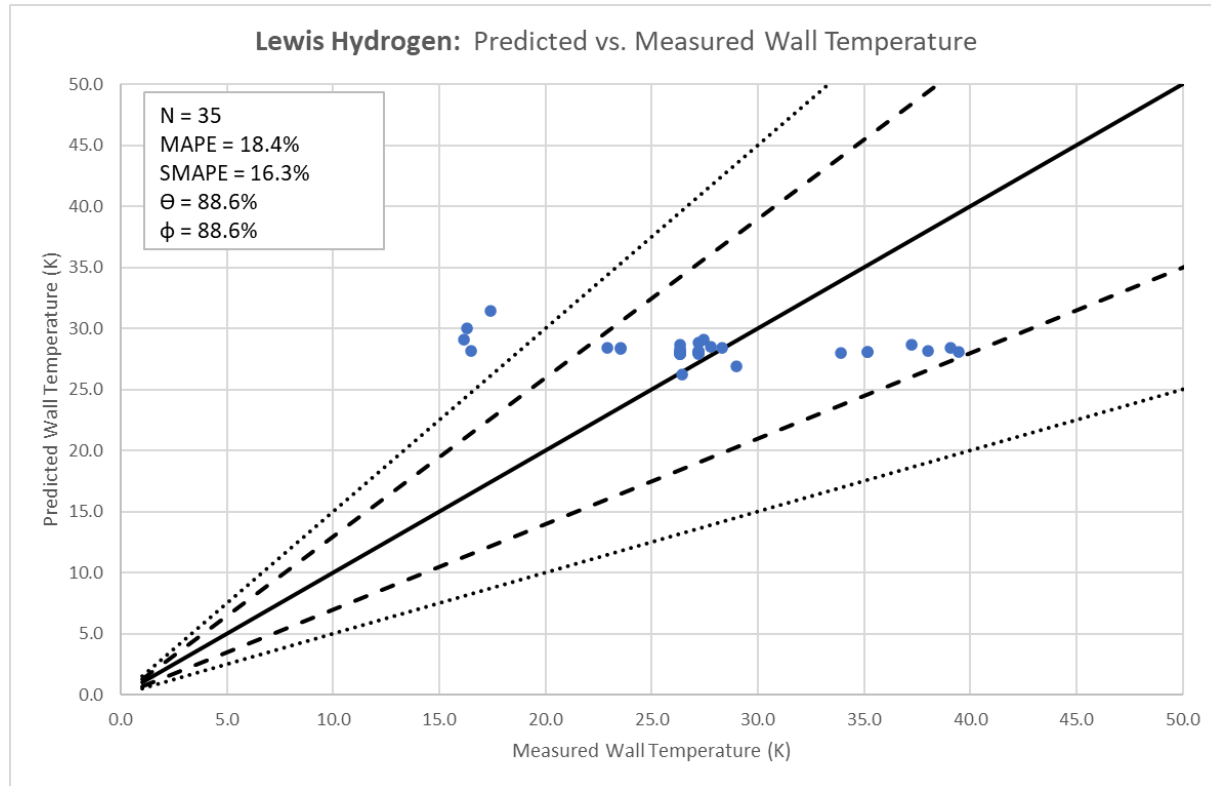
Finding ZCHF, MAPE = 47%



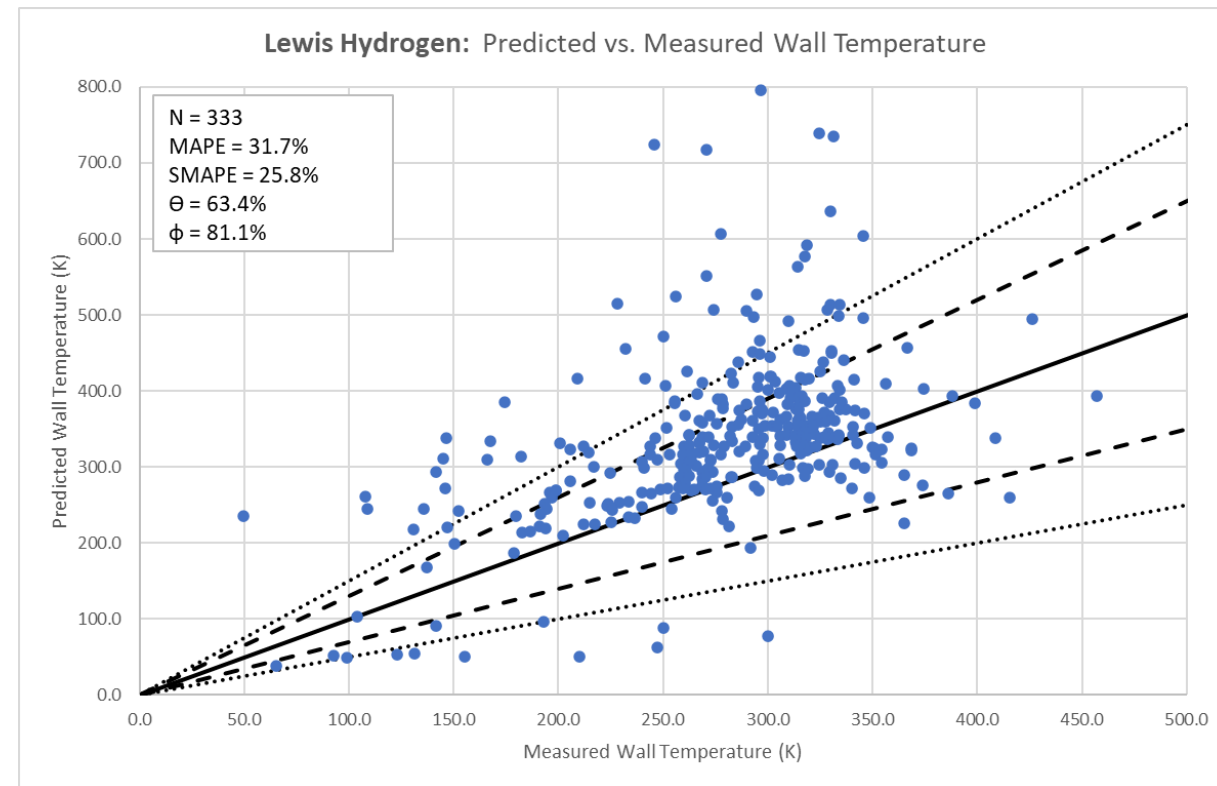
Fixing ZCHF, MAPE = 30%



# Lewis LH2 (1962), Parity Plots



Fixing  $Z_{CHF}$ , NB Only, MAPE = 18%



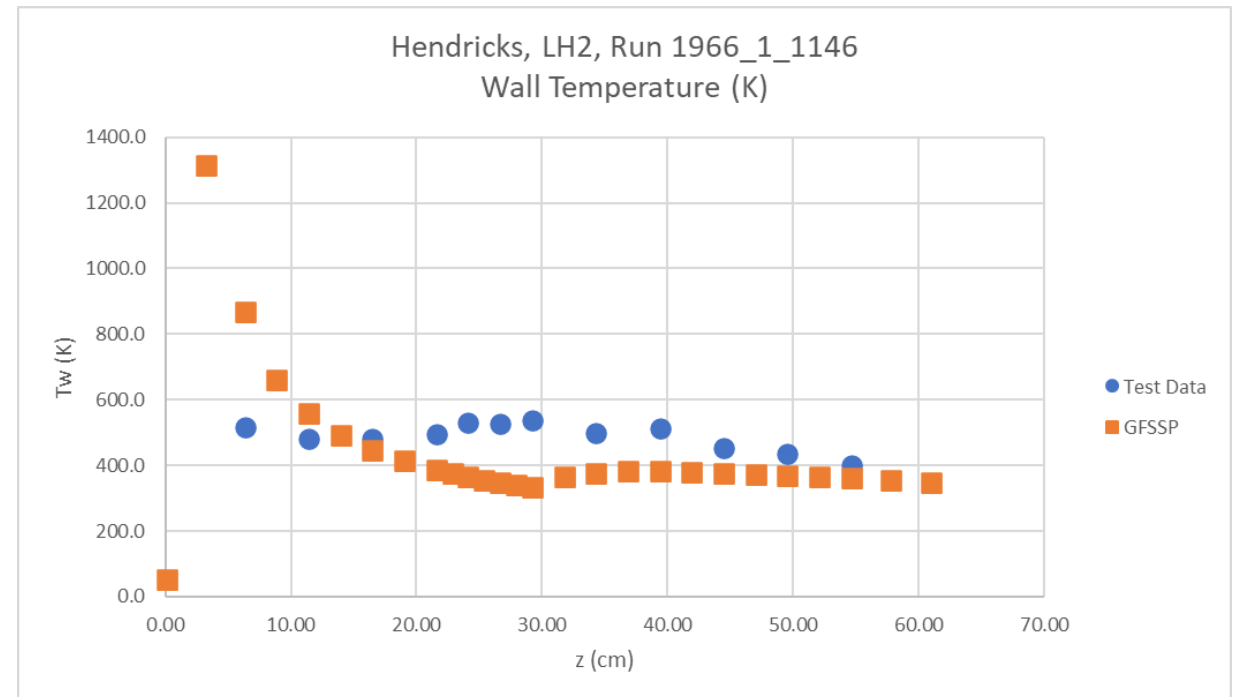
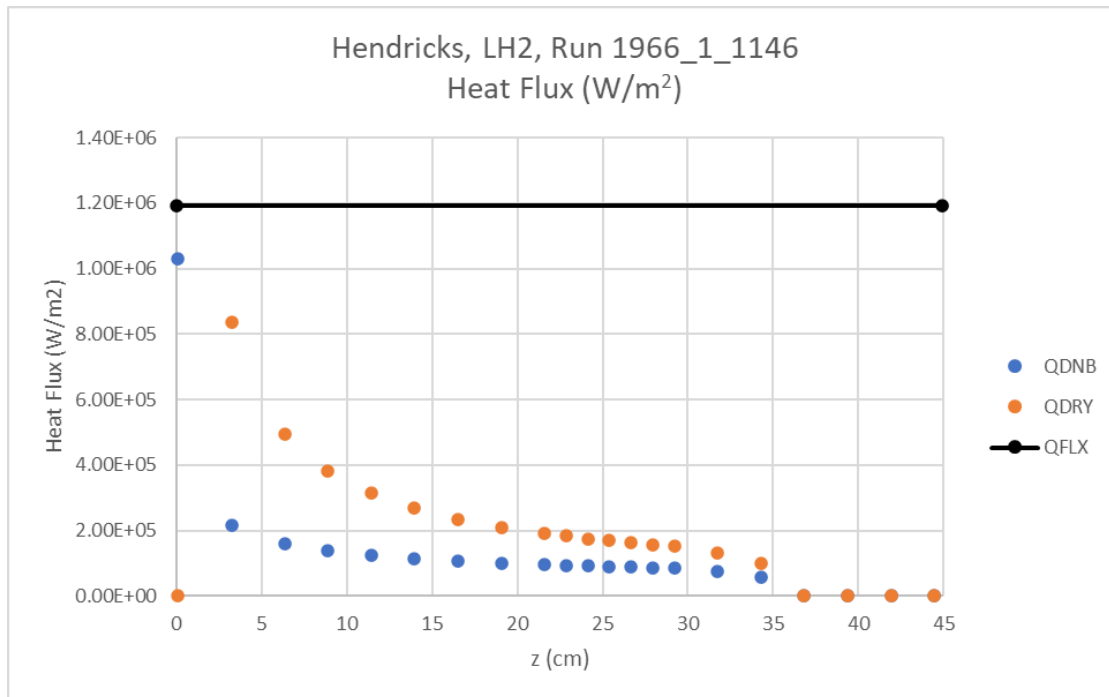
Fixing  $Z_{CHF}$ , FB Only, MAPE = 32%

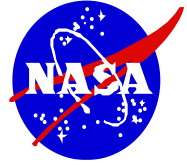
- When  $Z_{CHF}$  is fixed to the observed value, we can separate the NB and FB points.



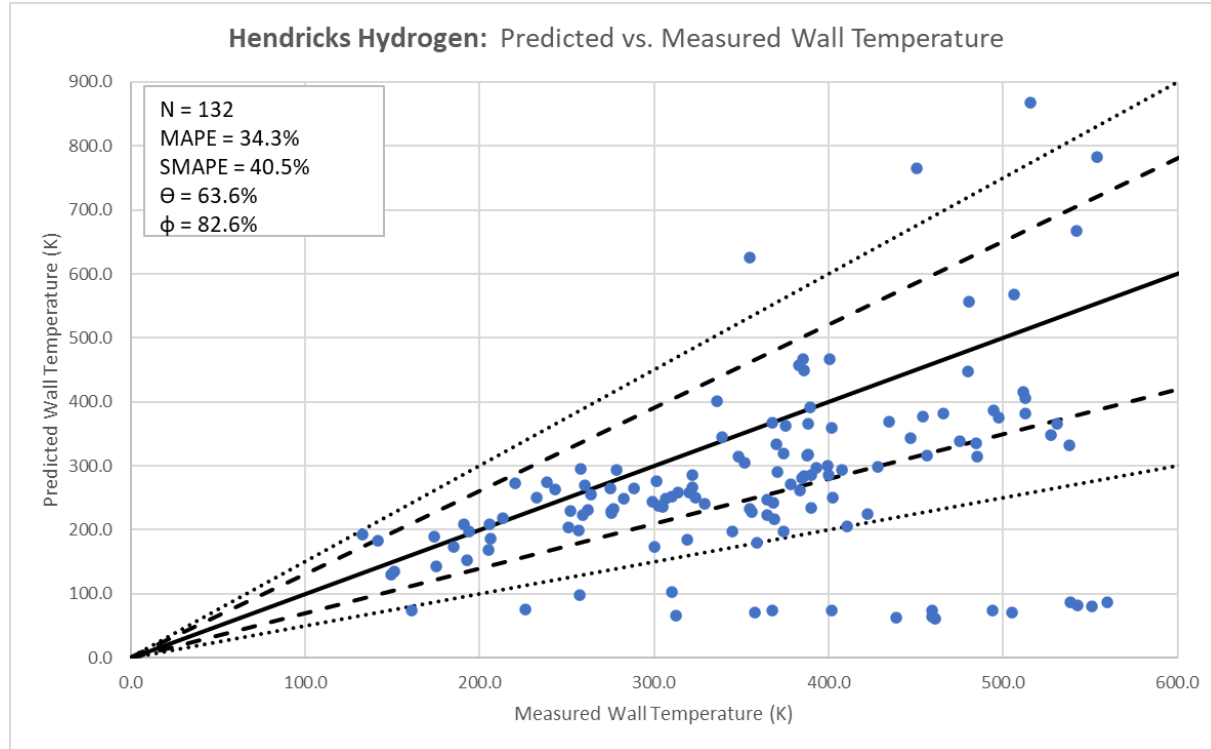
# Hendricks LH2 (1966)

- 11 runs
- L = 61 cm
- ID = 0.85-1.29 cm
- t = 0.025-0.081 cm
- Inconel or Stainless Steel
- P: 616-1113 kPa
- G: 327-1438 kg/m<sup>2</sup>-s
- Q: 735-2092 kW/m<sup>2</sup>

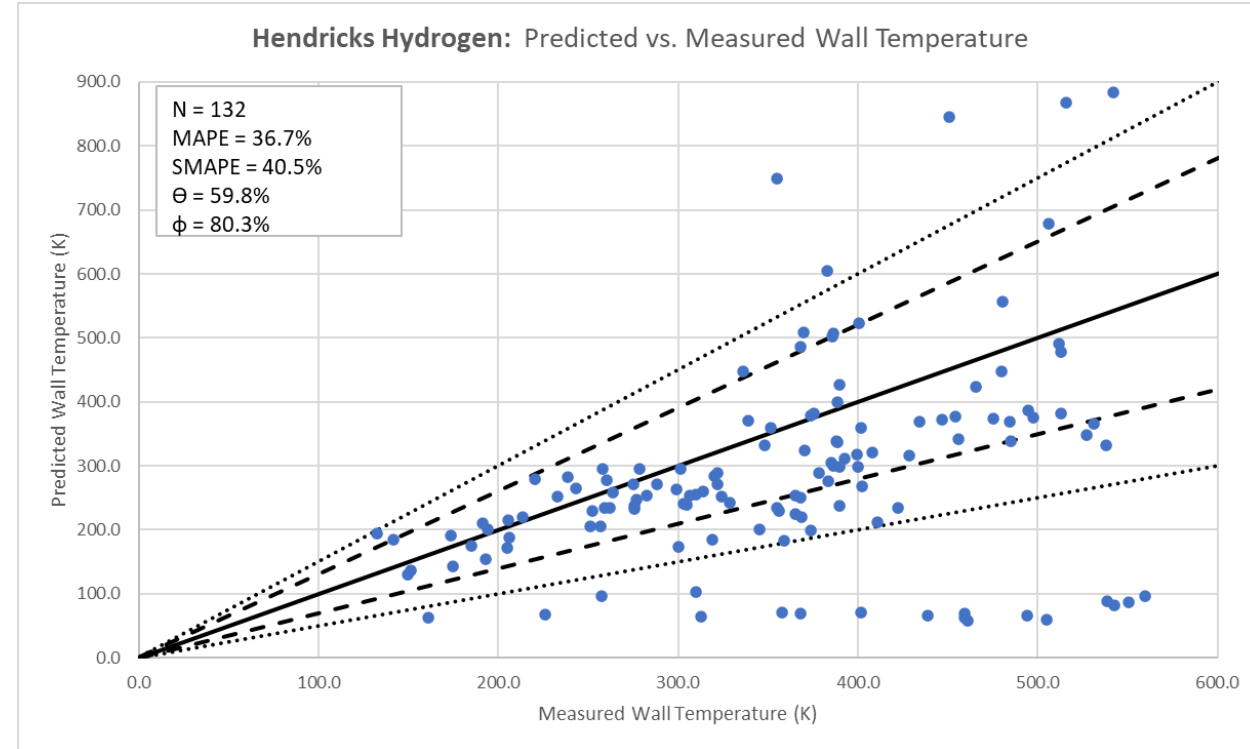




# Hendricks LH2 (1966), Parity Plots

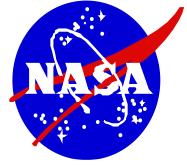


Finding ZCHF, MAPE = 34%

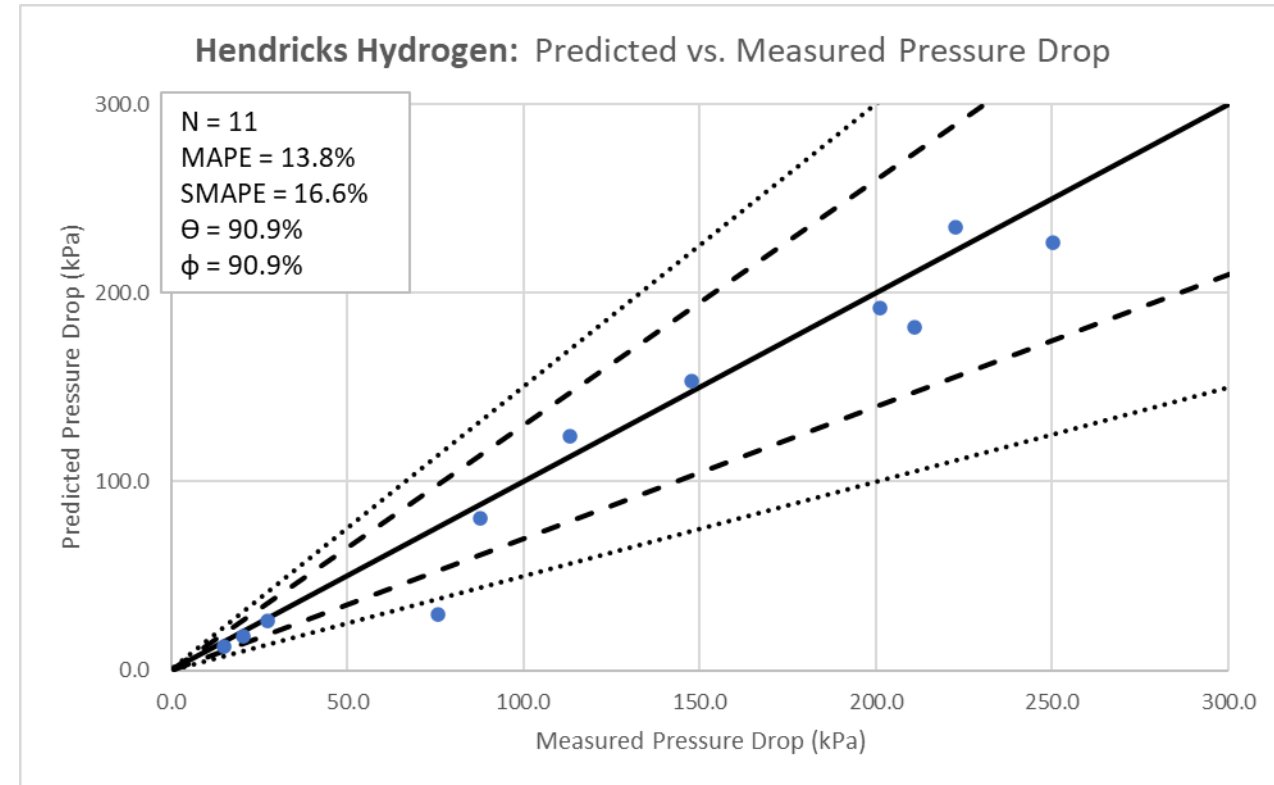
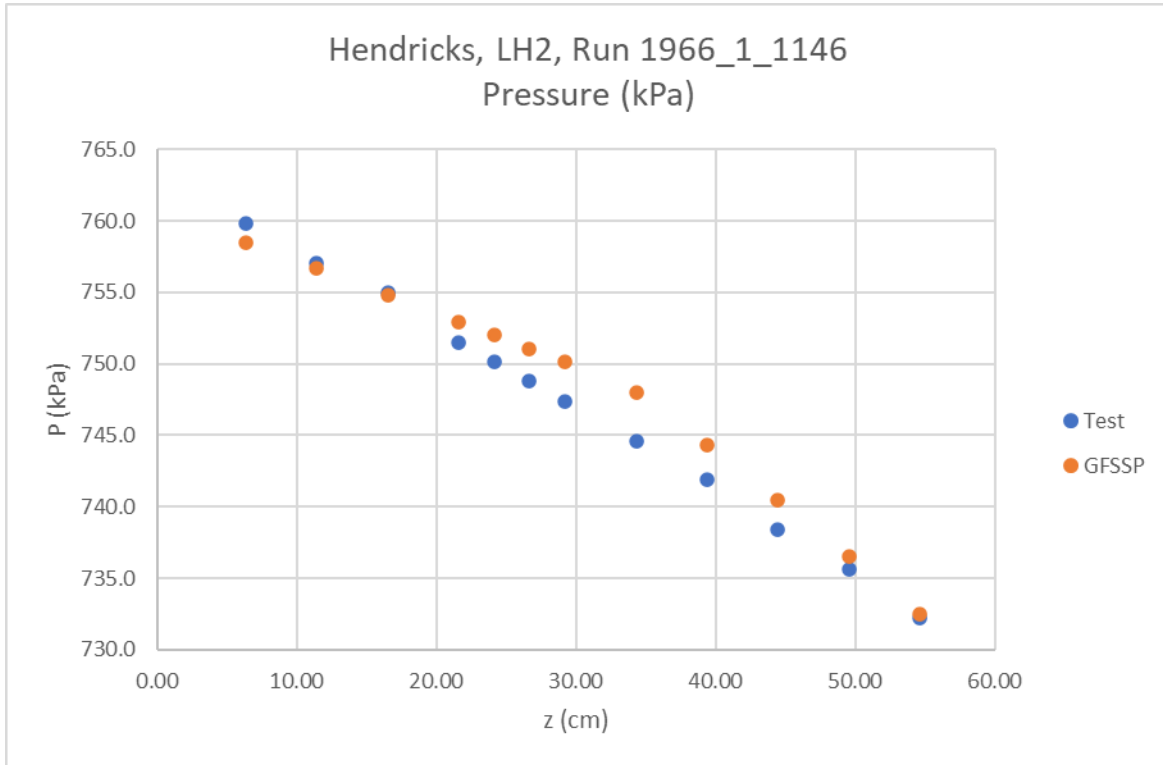


Fixing ZCHF, MAPE = 37%

- All test points are in the FB region.
- Most outliers are in the subcooled FB region.



# Hendricks LH2 (1966), Pressure Drop



- Pressure drop correlation includes
  - Friction (McAdams or Modified Lockhart-Martinelli)
  - Gravity
  - Acceleration

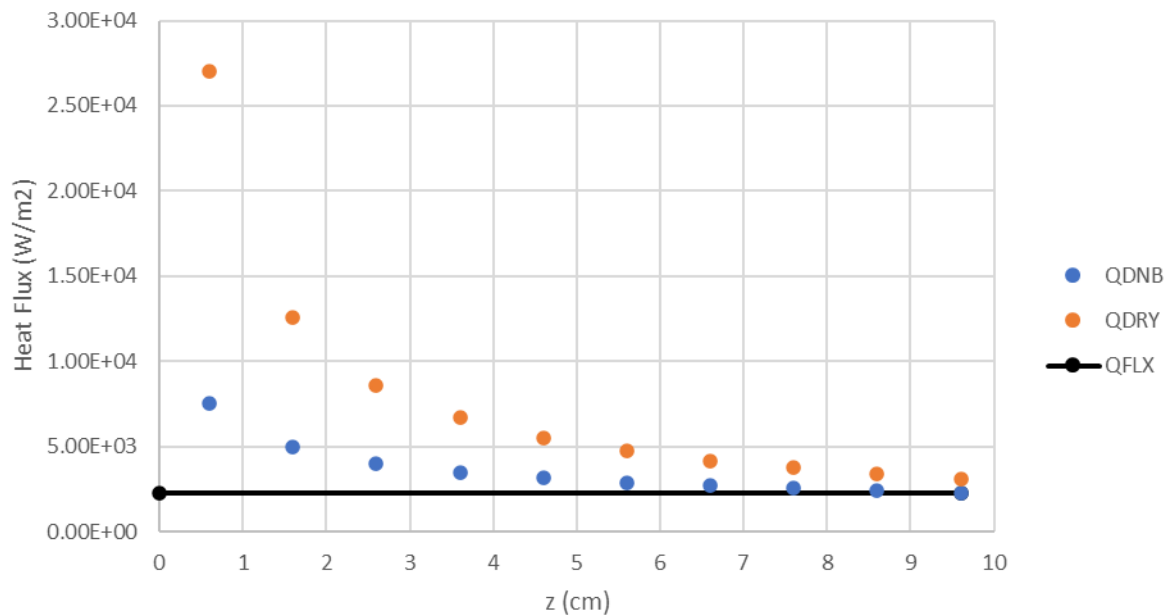


# Giarrantano LHe (1973)

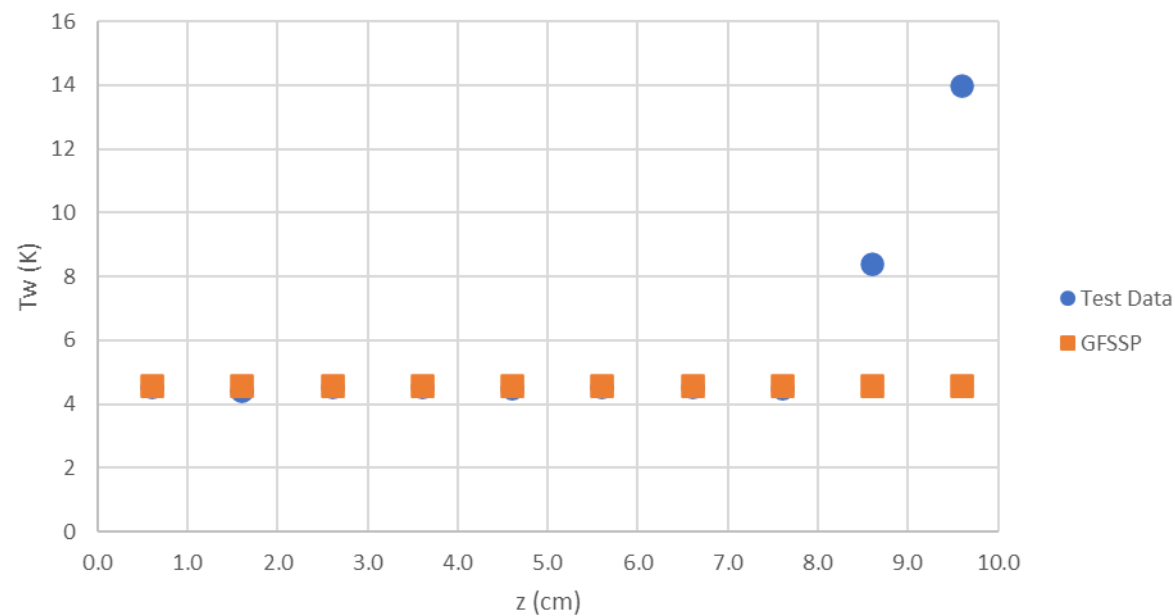
- 10 runs
- $L = 10$  cm
- $ID = 0.213$  cm
- $t = 0.016$  cm

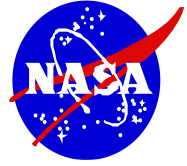
- Stainless Steel
- $P: 109-176$  kPa
- $G: 48-636$  kg/m<sup>2</sup>-s
- $Q: 0.6-5$  kW/m<sup>2</sup>

Giarrantano 1973, LHe, Run Fig3.1  
Heat Flux (W/m<sup>2</sup>)

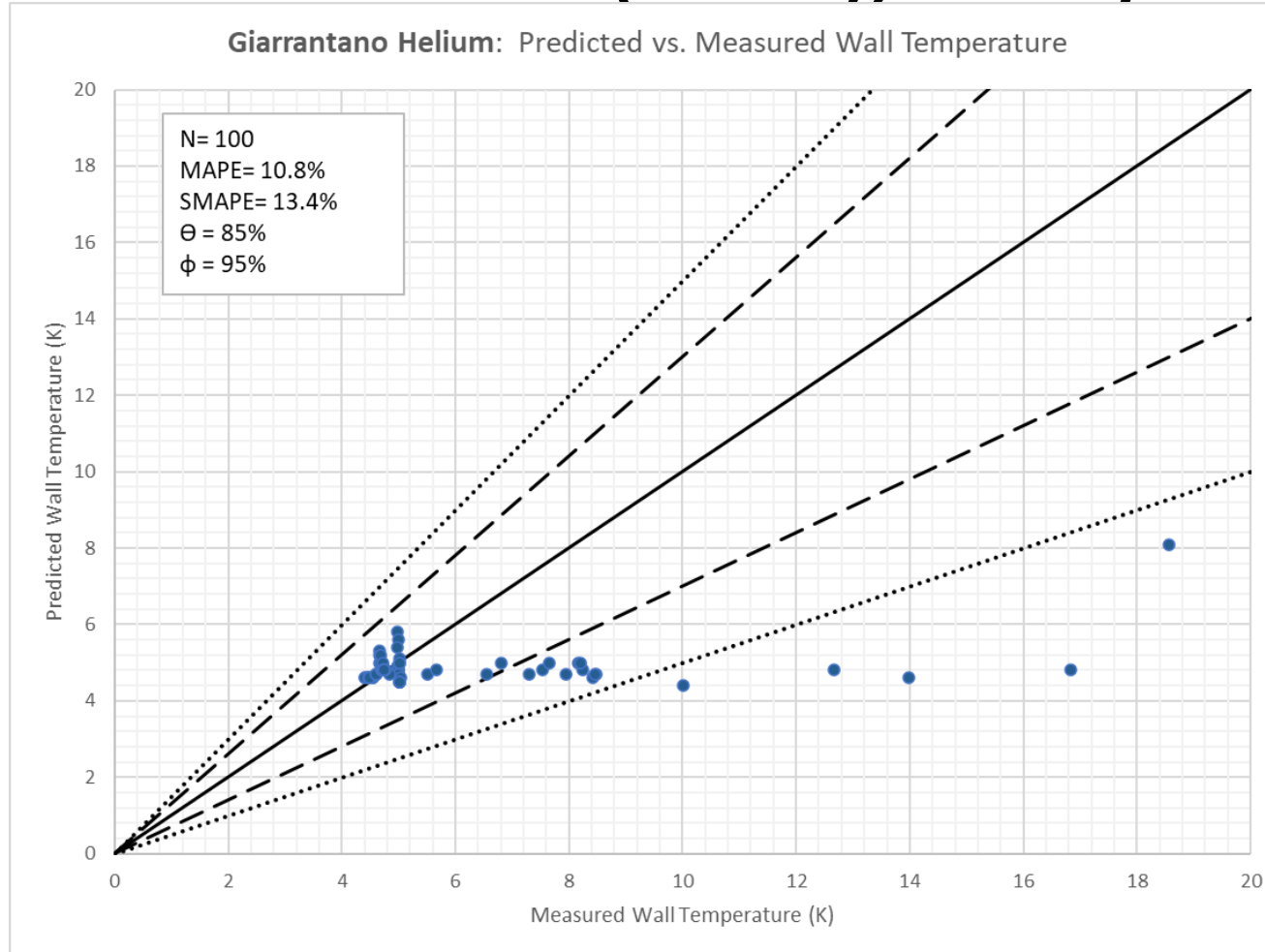


Giarrantano 1973, LHe, Run Fig3.1  
Wall Temperature (K)





# Giarrantano LHe (1973), Parity Plot



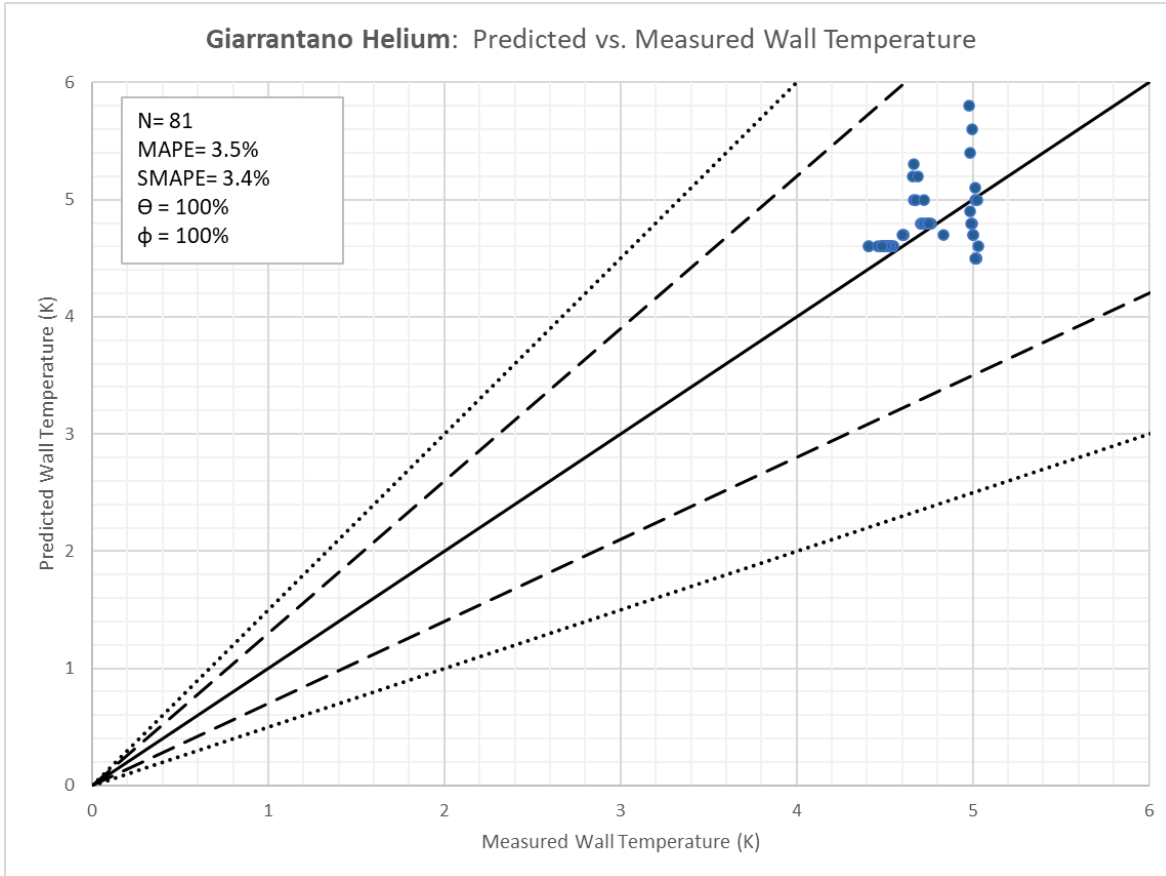
Finding ZCHF, MAPE = 11%

- Outliers occur where code predicted NB instead of FB.

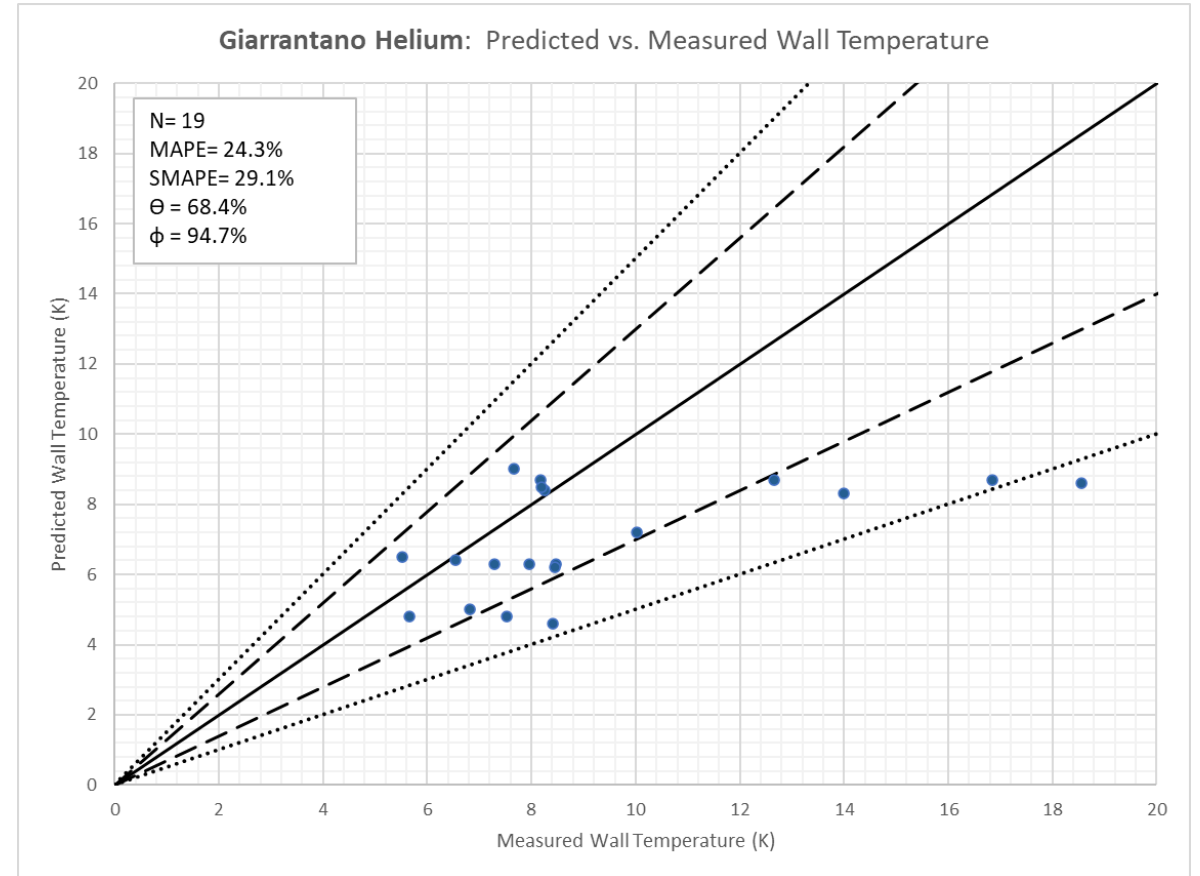




# Giarrantano LHe (1973), Parity Plots



Fixing ZCHF, NB, MAPE = 4%



Fixing ZCHF, FB, MAPE = 24%



# Conclusions

- The Purdue Universal Cryogenic Correlations are found to model LH2 and LHe boiling flows with reasonable accuracy in most phases.
- A method to determine the critical length  $Z_{CHF}$  when both DNB and DRY meet the criteria is needed.
- The development of a subcooled FB correlation is desirable.
- The Purdue correlations predict the FB region more accurately than the Miropolskii correlation.
- The Purdue two-phase pressure drop correlation appears to be accurate, but more testing is needed. Unfortunately, many experiments lack pressure drop data.