

ESTIMATION OF SOC OF LiFePO_4 CELLS USING A REDUCED ORDER MODEL WITH EXTENDED KALMAN FILTER

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Outline

Background

- SOC estimation and application
- Need for a reduced order model

Modeling of LFP cells and order reduction

- Modeling of LFP cells
- Order reduction
- Validation of the ROM

Design of EKF

- Principle of EKF
- Results of the ROM with EKF

Summary

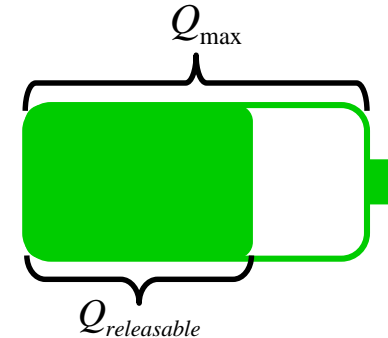


SOC estimation and application

Definition of SOC

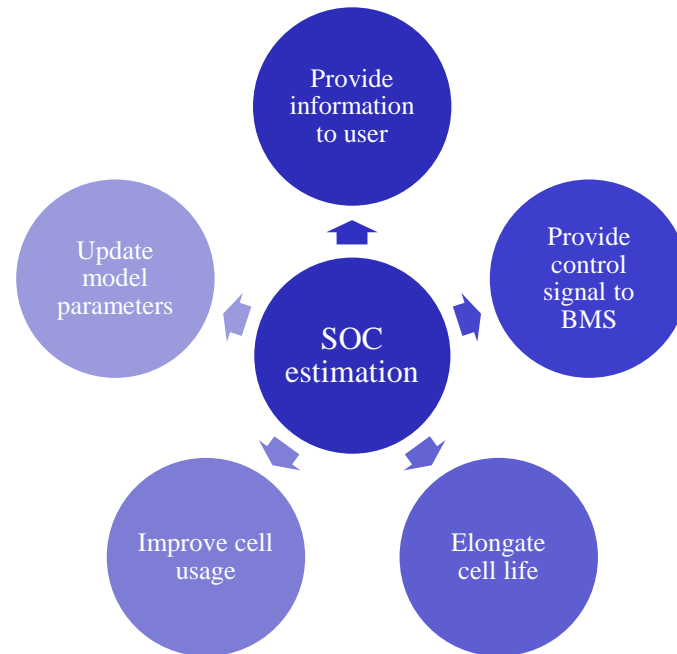
The ratio of releasable charges stored in a battery ($Q_{releasable}$) and the maximum capacity of the battery (Q_{max})

$$\rightarrow SOC = \frac{Q_{releasable}}{Q_{max}}$$



Application of SOC estimation

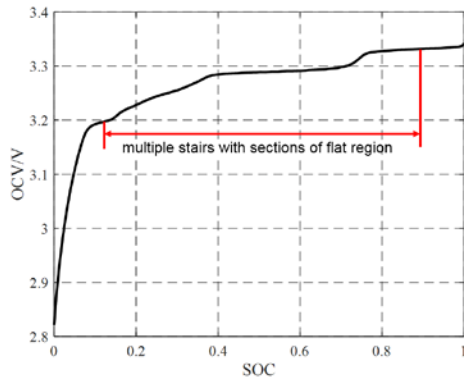
- ❖ Provide information to user
 - Available energy
 - Recharge
- ❖ Provide information to BMS
 - Energy management
 - Detect cell balancing
- ❖ Elongate cell life
 - Prevent overcharge
 - Prevent overdischarge
- ❖ Improve cell usage
 - Usage indication
- ❖ Update model parameters



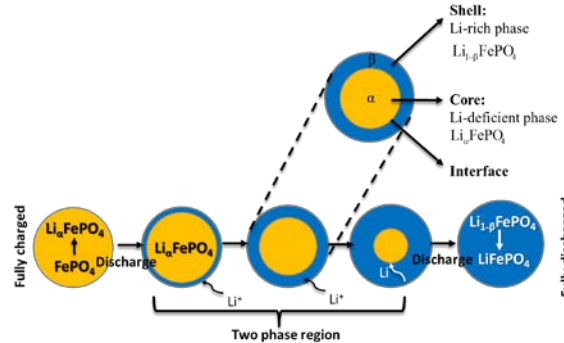
Need of a reduced order model

| Estimation method | Open loop SOC estimation | Closed loop SOC estimation with ECM | Closed loop SOC estimation with ROM |
|-------------------|---------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Pros | <ul style="list-style-type: none"> Minimum requirement of CPU | <ul style="list-style-type: none"> Simple model structure Can track SOC even if the initial condition is unknown | <ul style="list-style-type: none"> ✓ Accurately model the voltage plateau and path dependency ✓ Can track SOC even if the initial condition is unknown |
| Cons | <ul style="list-style-type: none"> Inaccurate estimation if initial SOC is unknown | <ul style="list-style-type: none"> Circuit components cannot reflect the physical states Inaccurate modeling for voltage plateau, phase transition and path dependency | <ul style="list-style-type: none"> • Complex modeling structure |

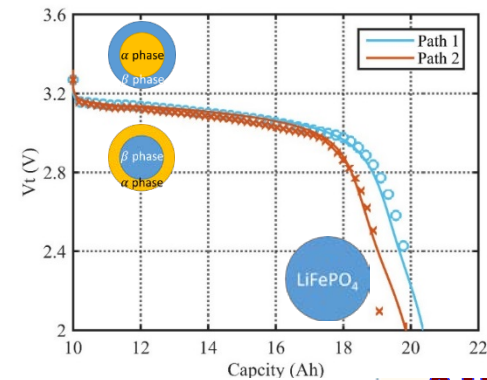
OCV characteristic of a LFP cell



Two phase transition

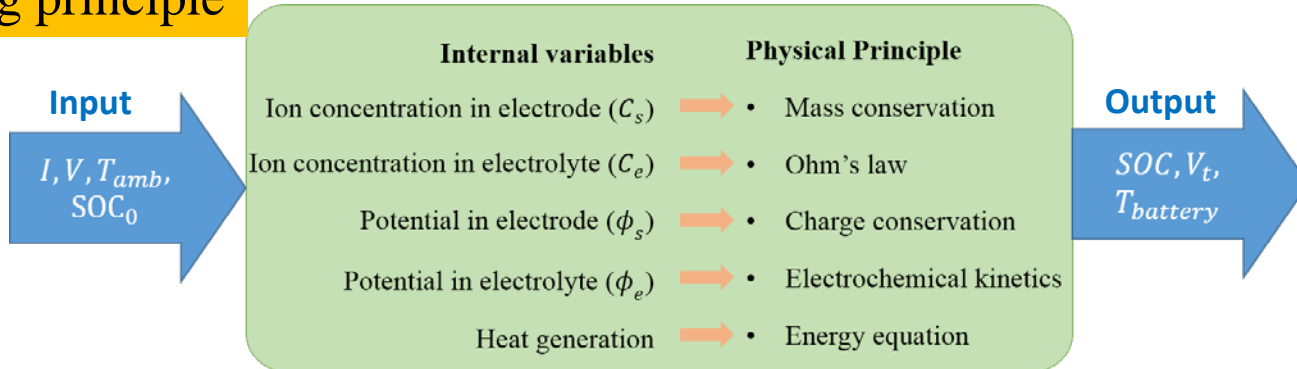


Path dependency

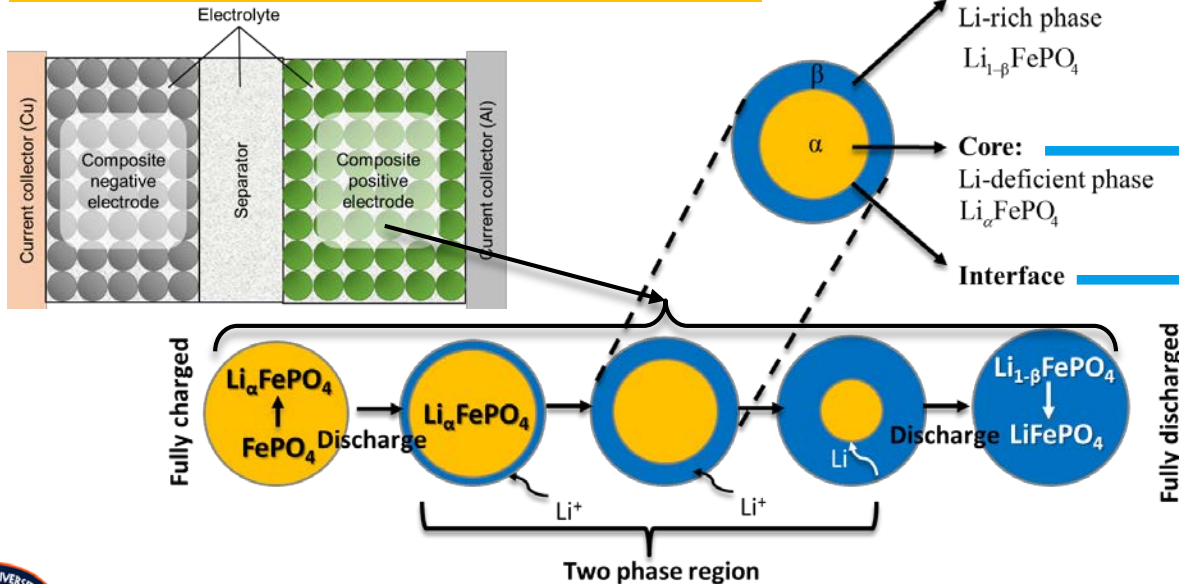


Modeling of LFP cells – Two phase transition

Modeling principle



Modeling of two phase transition



$$\text{Fick's law of diffusion: } \frac{\partial C_s}{\partial t} = \frac{D_{s,\beta}}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C_s}{\partial r} \right)$$

$$\text{Boundary condition: } D_{s,\beta} \frac{\partial C_s}{\partial r} \Big|_{r=R_s} = \frac{-j^{Li}}{a_s F}$$

$$\text{Fick's law of diffusion: } \frac{\partial C_s}{\partial t} = \frac{D_{s,\alpha}}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial C_s}{\partial r} \right)$$

$$\text{Boundary condition: } D_{s,\alpha} \frac{\partial C_s}{\partial r} \Big|_{r=0} = 0$$

Mass conservation in the control volume:

$$\text{Generation} = -(C_{\beta} - C_{\alpha}) dr_0$$

Flowin - Flowout =

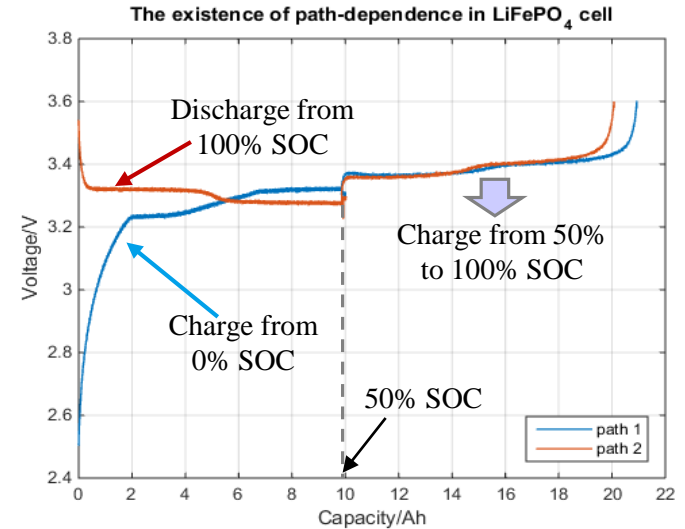
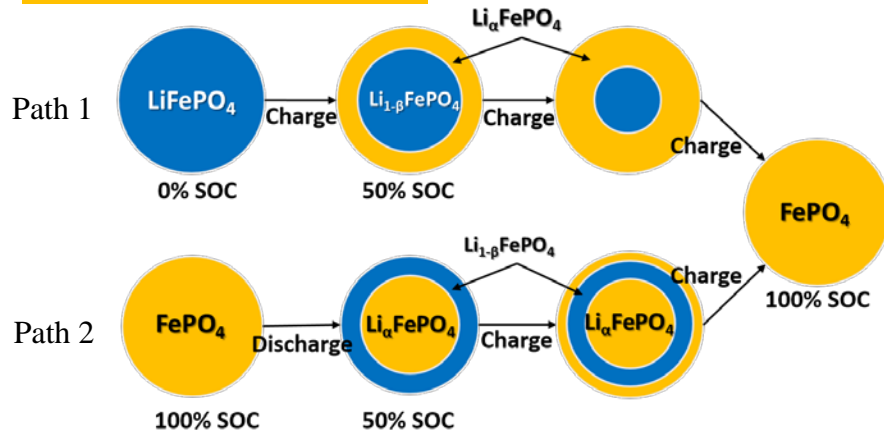
$$\left(D_{s,\beta} \frac{\partial C_{s,\beta}}{\partial r} \Big|_{r=r_0} - D_{s,\alpha} \frac{\partial C_{s,\alpha}}{\partial r} \Big|_{r=r_0} \right) dt$$

$$-(C_{\beta} - C_{\alpha}) \frac{dr_0}{dt} = D_{s,\beta} \frac{\partial C_{s,\beta}}{\partial r} \Big|_{r=r_0} - D_{s,\alpha} \frac{\partial C_{s,\alpha}}{\partial r} \Big|_{r=r_0}$$



Modeling of LFP cells - Path dependency

Path dependency



Validation of path dependency

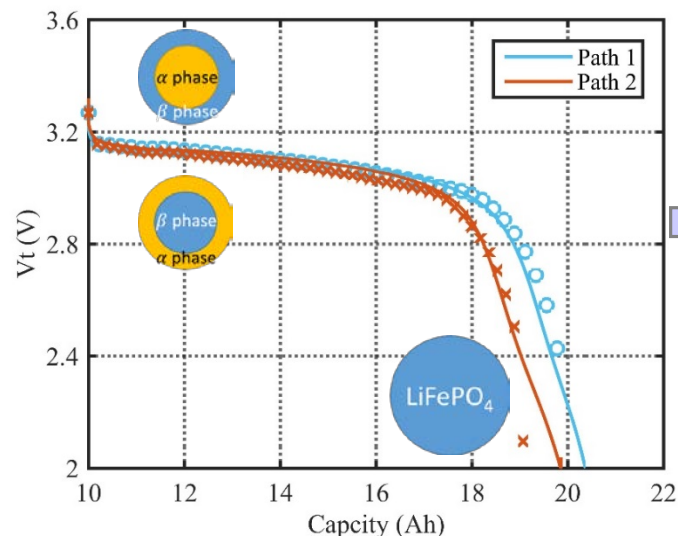
❖ Testing condition

• Path 1

Previously discharged with 0.1C from 100% to 50% SOC

• Path 2

Previously charged with 0.1C from 0% to 50% SOC



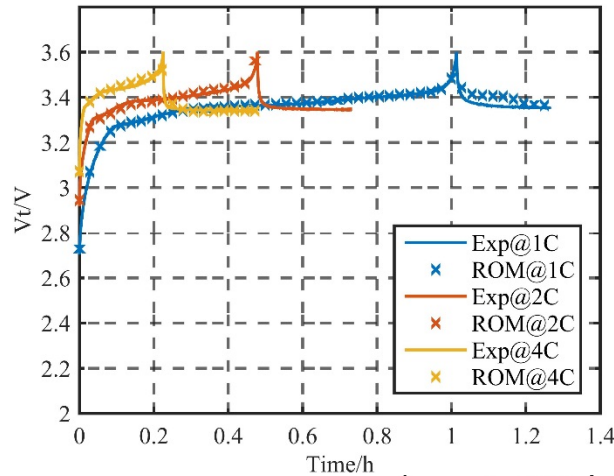
❖ Different path results in different releasable capacity.

Order reduction

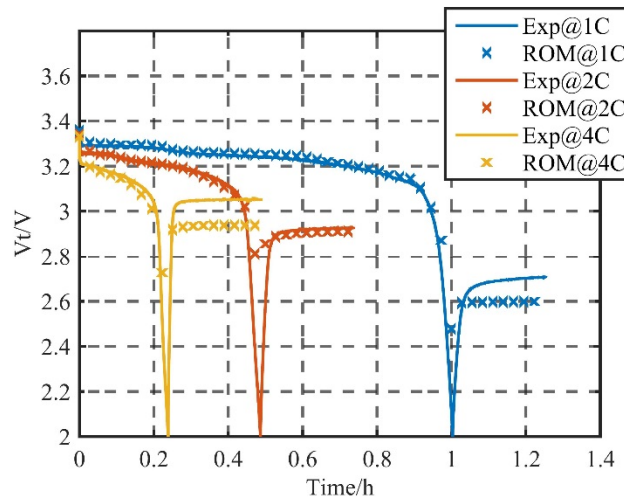
| | Full order model (FOM) | Reduction technique | Reduced order model (ROM) |
|-----------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Ion concentration in electrode | $\frac{\partial c_s}{\partial t} = \frac{D_{s,\beta}}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial c_s}{\partial r} \right); D_{s,\beta} \frac{\partial c_s}{\partial r} \Big _{r=r_1} = 0$ $\frac{\partial c_s}{\partial t} = \frac{D_{s,\alpha}}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial c_s}{\partial r} \right); D_{s,\alpha} \frac{\partial c_s}{\partial r} \Big _{r=R_s} = \frac{-j^{Li}}{a_s F}$ $(c_{s,\alpha\beta} - c_{s,\beta\alpha}) \frac{dr_0}{dt} = D_{s,\beta} \frac{\partial c_{s,\beta}}{\partial r} \Big _{r=r_0} - D_{s,\alpha} \frac{\partial c_{s,\alpha}}{\partial r} \Big _{r=r_0}$ | Polynomial approach | $\frac{d}{dt} c_{s,ave} - 3 \frac{D_s}{r_0^2} (35(c_{s,surf} - c_{s,ave}) - 8q_{ave} r_0) = 0$ $(c_{s,\beta\alpha} - c_{s,\alpha\beta}) \frac{dr_0}{dt} = -D_{s,\beta} \frac{(c_{s,surf} - c_{s,\beta\alpha})k_2 - (c_{s,surf} - c_{s,\beta\alpha})k_4}{k_2 k_3 - k_1 k_4}$ $+ \frac{D_s}{r_0} (35(c_{s,surf} - c_{s,ave}) - 8q_{ave} r_0)$ |
| Ion concentration in electrolyte | $\frac{\partial(\epsilon_e c_e)}{\partial t} = \frac{\partial}{\partial x} \left(D_e^{eff} \frac{\partial}{\partial x} c_e \right) + \frac{1-t_+^0}{F} j^{Li}$ $\frac{\partial c_e}{\partial t} \Big _{x=0} = \frac{\partial c_e}{\partial t} \Big _{x=L} = 0$ | Residual grouping | $\dot{c}_e = \hat{A} \cdot c_e + \hat{B} \cdot I$ $y = \hat{C} \cdot c_e + \hat{D} \cdot I$ |
| Ohm's law in electrolyte | $\frac{\partial}{\partial x} \left(\kappa^{eff} \frac{\partial}{\partial x} \phi_e \right) + \frac{\partial}{\partial x} \left(\kappa_D^{eff} \frac{\partial}{\partial x} \ln c_e \right) + j^{Li} = 0$ $\frac{\partial \phi_e}{\partial x} \Big _{x=0} = \frac{\partial \phi_e}{\partial x} \Big _{x=L} = 0$ | C_e has no influence on reaction current | $\frac{\partial}{\partial x} \left(\kappa^{eff} \frac{\partial \phi_e}{\partial x} \right) + j^{Li} = 0$ |
| Electrochemical kinetics | $j^{Li} = a_s i_0 \left\{ \exp \left[\frac{\alpha_a F}{RT} \eta \right] - \exp \left[-\frac{\alpha_c F}{RT} \eta \right] \right\}$ $\eta = \phi_s - \phi_e - U$ | Linearization | $\frac{\partial}{\partial x} \left(\frac{\partial}{\partial x} \phi_{se} \right) = j^{Li} \left(\frac{1}{\sigma^{eff}} + \frac{1}{\kappa^{eff}} \right)$ $j^{Li} = \frac{a_s i_0 F}{RT} (\phi_{se} - U)$ |

Validation of ROM

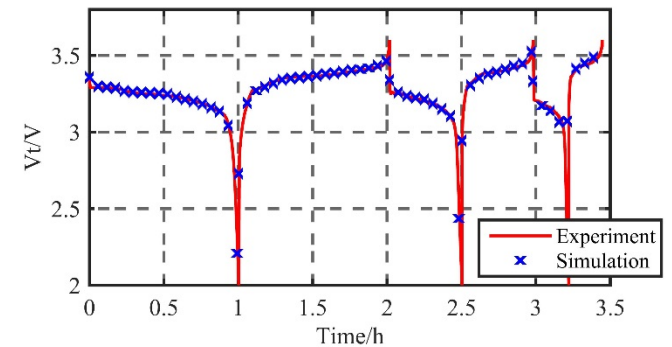
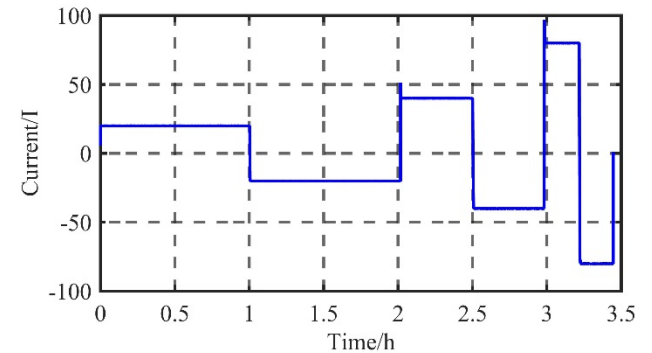
Test condition:
 Profile: CC charge
 Temperature: 25°C
 Current: 1C, 2C, 4C
 Initial SOC: 0%



Test condition:
 Profile: CC discharge
 Temperature: 25°C
 Current: 1C, 2C, 4C
 Initial SOC: 100%

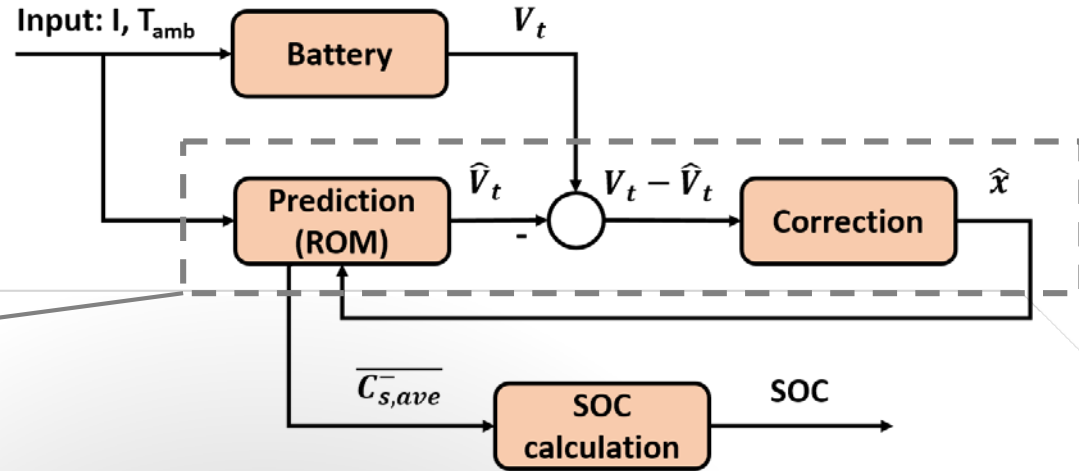


Test condition:
 Profile: Multiple cycle
 Temperature: 25°C
 Current: 1C, 2C, 4C
 Initial SOC: 100%



Principle of EKF

Working principle of EKF Based on ROM:



EKF Algorithm

Battery Model

$$\mathbf{x}_k = f(\mathbf{x}_{k-1}, \mathbf{u}_{k-1}, \mathbf{w}_{k-1})$$

$$\mathbf{z}_k = h(\mathbf{x}_k, \mathbf{v}_k)$$

Initialization

State Estimation:
 $\hat{\mathbf{x}}_0$
 Error Covariance:
 P_0

Time Update (Prediction)

State:
 $\hat{\mathbf{x}}_k^- = f(\hat{\mathbf{x}}_{k-1}^-, u_{k-1}, 0)$
 Error Covariance:
 $P_k^- = A_k P_{k-1} A_k^T + W_k Q_{k-1} W_k^T$

Measurement Update (Correction)

Kalman Gain:
 $K_k = P_k^- H_k^T (H_k P_k^- H_k^T + V_k P_{k-1} V_k^T)^{-1}$
 State:
 $\hat{\mathbf{x}}_k = \hat{\mathbf{x}}_k^- + K_k (z_k - h(\hat{\mathbf{x}}_k^-, 0))$
 Error Covariance
 $P_k = (I - K_k H_k) P_k^-$

Flowchart of SOC Estimation Process

State: $x = [c_{s,ave}^-]$
Measurement: $y = [V_t]$

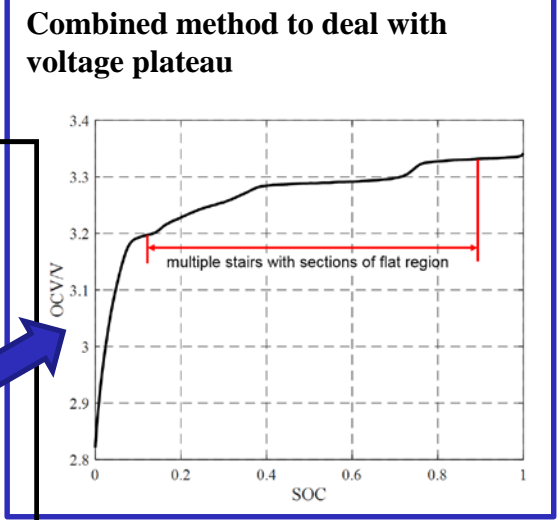
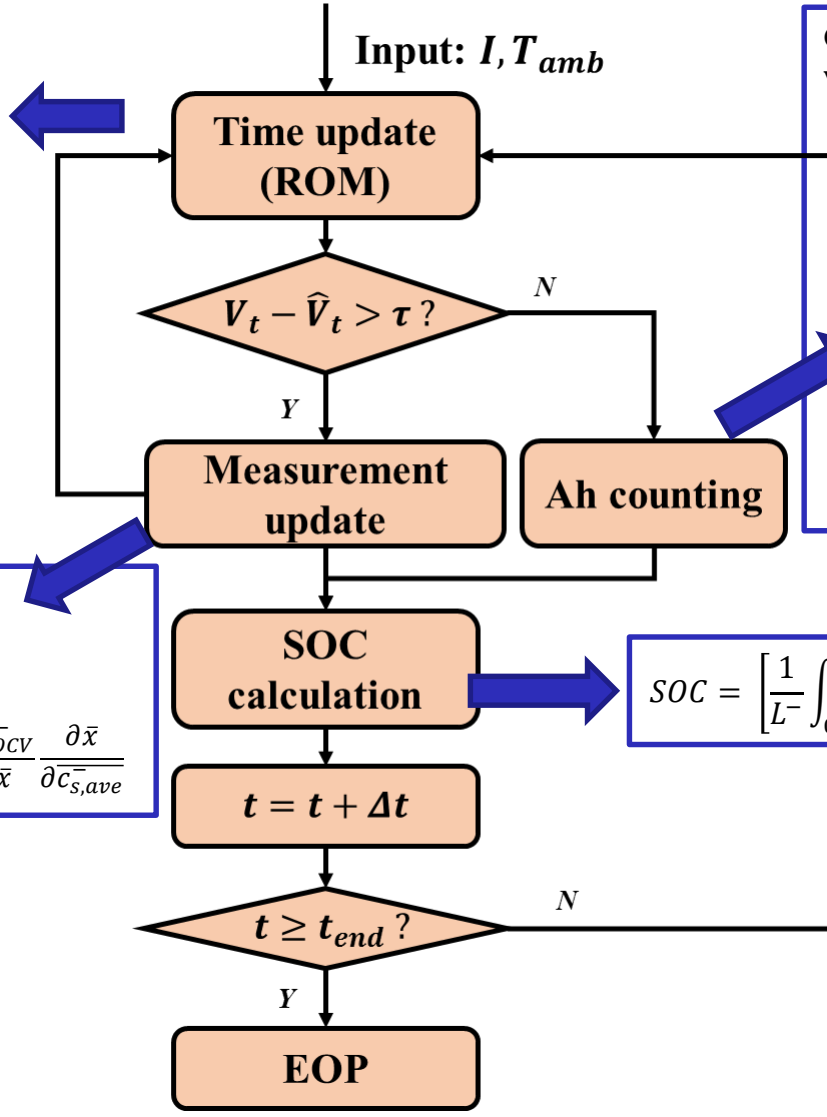
Model Reformulation:

$$\overline{c_{s,ave}^-}^k = \overline{c_{s,ave}^-}^{k-1} - 3 \frac{j^{Li}}{R_s a_s F A L^-} I$$

$$V_t = U^+(\bar{y}) - U^-(\bar{x}) - \eta$$

Jacobians:

$$A = \frac{\partial \overline{c_{s,ave}^-}^k}{\partial \overline{c_{s,ave}^-}^{k-1}} = I$$

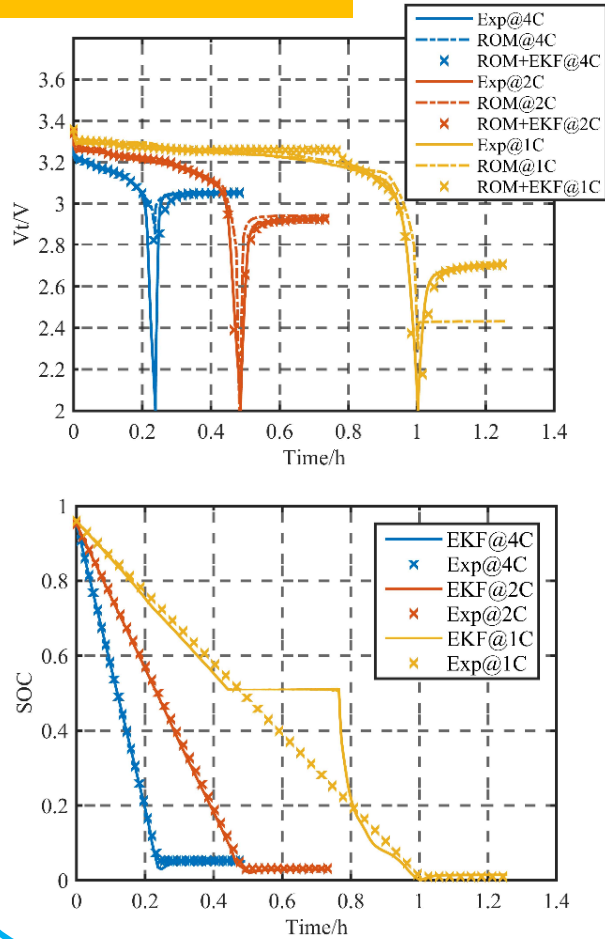
$$H = \frac{\partial V_t}{\partial \overline{c_{s,ave}^-}} = \frac{\partial U_{OCV}^+}{\partial \bar{y}} \frac{\partial \bar{y}}{\partial c_{s,ave}^+} \frac{\partial \overline{c_{s,ave}^-}}{\partial c_{s,ave}^-} - \frac{\partial U_{OCV}^-}{\partial \bar{x}} \frac{\partial \bar{x}}{\partial \overline{c_{s,ave}^-}}$$


$$SOC = \left[\frac{1}{L^-} \int_0^{L^-} \frac{c_{s,ave-} - c_{s,max} \cdot x_0}{c_{s,max}(x_{100} - x_0)} dx \right] \cdot 100\%$$

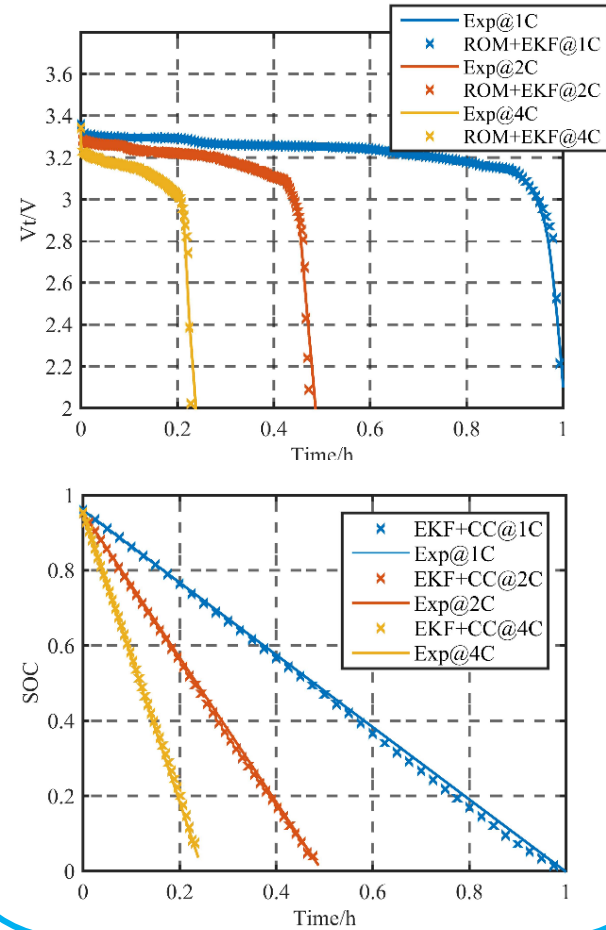


Result of ROM with EKF

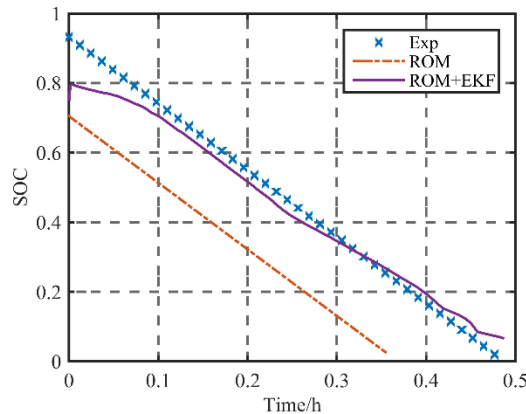
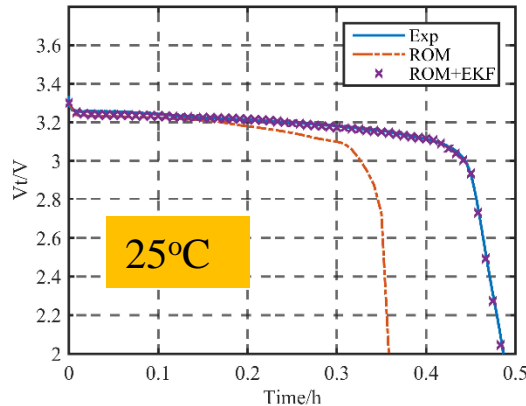
ROM with EKF



ROM with Combined method

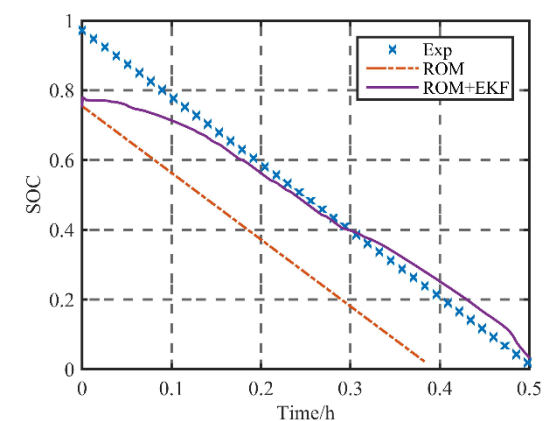
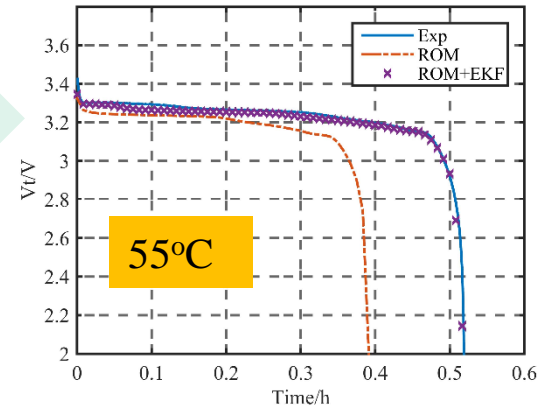
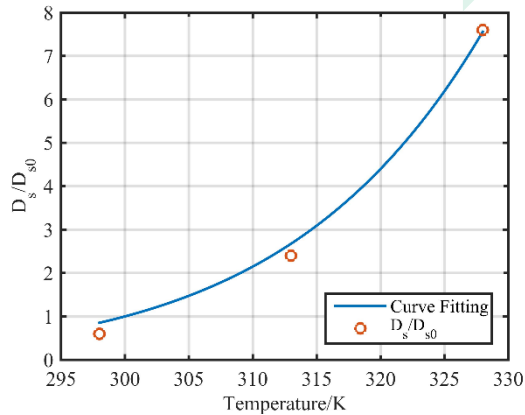


Validation of ROM + EKF (with initial error and temperature dependency)



Arrhenius equation

$$D_s = D_{s0} \cdot \exp\left(\frac{E_a}{R} \left(\frac{1}{T_0} - \frac{1}{T}\right)\right)$$



- ❖ Test condition: 2C-rate CC discharge at 25°C.
- ❖ 20% initial SOC error (0.2V terminal voltage error) is assumed.
- ❖ The initial error can be corrected with EKF.

Summary

□ Summary

- Development of ROM for LiFePO_4 cells considering **two phase transition** and **path dependency**.
- Development of **combined EKF algorithm** for SOC estimation.
- Comparison of simulation results of combined algorithm and tradition EKF and their analysis under different operation conditions.

□ Conclusion

- The combined algorithm shows a better SOC estimation result.

□ Future work

- Incorporation of **thermal model**.
- Validation of **drive cycle** profiles



Thanks for your attention!

